Adsorption of Mercury Ion From Aqueous Solutions Onto Bentonite Clay

آمتزاز ايون الزئبق من محاليله المائية على طين البنتونايت

Assistant Lecture / Mouhannd H. Naji / Department of Chemistry / College of Science / Kufa

University

Email : mohanndhn@sci.kuiraq.com

Abstract:

In this research, the bentonite clay was utilized for the removal of mercury ion from aqueous solutions. Adsorption experiments were conducted under various conditions where the batch method was used to determine the best adsorption ratio and the adsorption capacity for the concentration used of Hg(II) ion between (100-10 mg/L), the results show that the best concentration was (10 mg/L) where the adsorption ratio was 88.7 and the adsorption capacity was 0.444 mg/g. The adsorbent dose was 20 g/L, and the shaking time found that it equal to 140 min and the best pH value between (5-8). The effect of temperature and thermodynamic functions wear also studied, the adsorption capacity was increased with increased the temperature and the reaction was endothermic. The equilibrium isotherm data was analyzed using the Langmuir equation, where found q_m and *b* are equal to 3.367 mg/g and 0.134 respectively. The rate constant k_2 for the adsorption of Hg(II) ion is equal to 0.1067 g/mg.min.

الخلاصة: في هذا البحث، أستعمل طين البنتونايت لإزالة أيون الزئبق الثنائي من محاليله المائية . تم اجراء تجارب الامتزاز تحت ظروف مختلفة حيث استعملت طريقة الدفعات لتقدير أفضل نسبة امتزاز وسعة امتزاز للتراكيز المستعملة لأيون الزئبق الثنائي والتي تراوحت ما بين (100-10 مليغرام/لتر)، فأظهرت النتائج ان أفضل تركيز كان (10 مليغرام/لتر) حيث كانت نسبة الامتزاز 7.88 وسعة الامتزاز 0.444 غرام/لتر)، فأظهرت النتائج ان أفضل تركيز كان (10 مليغرام/لتر) حيث كانت نسبة الامتزاز 7.88 وسعة الامتزاز 0.444 غرام/لتر)، عماني وجرعة الامتزاز كانت 20 غم/لتر , ووجد أن زمن الرج مساوي إلى معة الامتزاز تزداد بزيادة درجة الحرارة والتفاعل من النوع الماص للحرارة . تم تحليل بيانات أيزوني مالتران باستعمال معادلة لانكمير، حيث وجد ان m و d مساوية إلى 3.367 غرام/مليغرام و0.134 مالتران باستعمال أيون الكوبلت الثنائي مساوي إلى 0.106 غرام/مليغرام. ويقيقية .

Keywords: The bentonite clay, mercury ion, adsorption, batch method, Langmuir isotherm and the rate constant.

Introduction:

The presence of heavy metals in aqueous solution beyond certain limit creates serious threat to the environment because of their non-degradability and toxicity ⁽¹⁾. Mercury has many negative effects on human beings, such as the disruption of the nervous system, defects in the work and functions of the brain, distorting of DNA and chromosomes, and skin rashes because of allergies ⁽²⁾. Mercury metal has many uses because of its high density it is used in barometers and manometers, it is extensively used in thermometers and its ease in amalgamating with gold is used in the recovery of gold from its ores ⁽³⁾. Industry uses mercury metal as a liquid electrode in the manufacture of chlorine and sodium hydroxide by electrolysis of brine ⁽⁴⁾. Mercury is still used in some electrical gear, such as switches and rectifiers, which need to be reliable, and for industrial catalysis ⁽⁵⁾. Much less mercury is now used in consumer batteries and fluorescent lighting, but it has not been entirely eliminated ⁽⁶⁾.

Several methods are available to uptake toxic metals from aqueous solutions such as chemical precipitation ⁽⁷⁾, electrolysis (membrane separation) ⁽⁸⁾, ion exchange resins⁽⁹⁾, solvent extraction ⁽¹⁰⁾, reverse osmosis ⁽¹¹⁾, photoreduction ⁽¹²⁾ and adsorption⁽¹³⁾. Adsorption is generally efficient in the removal and recovery of heavy metal ions because of their physical and chemical stabilities, different conventional and non-conventional type of adsorbents have been used for removal of mercury ions, such as, activated carbon ⁽¹⁴⁾, tree fern ⁽¹⁵⁾, montmorillonite clay ⁽¹⁶⁾, Camel bone charcoal ⁽¹⁷⁾, corn cobs ⁽¹⁸⁾, etc.

Bentonite clay is widely applied in many fields of adsorption technology including the removal of metals ions $^{(19,20)}$, phenols $^{(21-23)}$, organic molecules $^{(24,25)}$, polymers $^{(26,27)}$, pesticides $^{(28)}$, radionuclides $^{(29)}$ and dyes $^{(30,31)}$. Bentonite, which is predominantly montmorillonite clay, is characterized by one Al octahedral sheet placed between two Si tetrahedral sheets. The isomorphous substitution of Al³⁺ for Si⁴⁺ in the tetrahedral layer and Mg²⁺ for Al³⁺ in the octahedral layer results in a net negative surface charge on the bentonite. This charge imbalance is offset by exchangeable cations (Na⁺ and Ca²⁺, etc.) at the bentonite surface. The layered structure of the clay expands after wetting. Na⁺ and Ca²⁺ are strongly hydrated in the presence of water, resulting in a hydrophilic environment at the bentonite surface $^{(32)}$.

The aim of the present work was to study the possibility of utilizing bentonite clay for the adsorption of mercury ions from aqueous solutions under various conditions.

Experimental Section:

1- Apparatus:

- 1- Spectrophotometer- PD-303, Japan.
- 2- Shaker Bath, SB-16, England.
- 3- pH-meter model Ionlop-720, Japan.
- 4- Oven, memmert $30C^{0}-220C^{0}$, W.Germany.
- 5- Centrifuge machine, Hettich EBA35, Japan.

2- Adsorbent preparation:

Bentonite clay used in this study was obtained from the Geological Survey of the Ministry of Industry and Minerals, Baghdad, Iraq. It was washed with an excess amount of distilled water to remove carbonate and remove the soluble materials. Then it was dried in the oven at $105C^{0}$ for (12h), the chemical analysis of bentonite clay is listed in Table (1)⁽³³⁾.

3- Preparation stock solution of Hg(II) (1000 mg/L):

A standard solution of 1000 mg/L of mercury ion was prepared by dissolving 0.1353 g of HgCl₂ in a minimum amount of distilled water in a 100 ml volumetric flask and the volume was made up to the mark with distilled water. Solutions of different concentrations were prepared by serial dilutions for mercury ion between (100-0.1 mg/L).

4- Adsorption studies:

Batch adsorption studies were carried out by adding (0.5 g) of bentonite clay to 25 ml of Hg(II) solution and shaken was done by a shaker bath. The pH of the solution was adjusted by adding dilute HCl or NaOH solution. At regular intervals 5 ml samples were withdrawn and filtered. The residual concentration in the solution was estimated colorimetrically with dithizone as orange-yellow dithizonate which is extractable into $CC1_4$ at λ_{max} equal to 485 nm ⁽³⁴⁾. From the Hg(II) concentrations measured before and after the adsorption (C_i and C_e, mg/L, respectively) and weight of bentonite clay (m, g), as well as volume of aqueous solution (V, L), the percentage of adsorption (% Adsorption) and the equilibrium adsorption capacity of mercury ion (q_e, mg/g) were calculated according to equations (1) and (2):

according to equations (1) and (2): % Adsorption = $\frac{C_i - C_e}{C_i} \times 100$ (1) $q_e = \frac{(C_i - C_e)V}{m}$ (2)

Results and Discussion:

1- Effect of initial concentration and adsorbent dose:

The effect of initial Hg(II) concentration on the adsorption ratio was studied by varying the initial Hg(II) concentration between (100-10) mg/L. It is observed that the percentage of adsorption increased from 57.4 to 88.7 and the adsorption capacity decreased from 2.87 to 0.444 mg/g when the concentration decreased from 100 to 10 mg/L, the result show that the best concentration of Hg (II) was given the best adsorption ratio was 10 mg/L. From the results, noted the adsorption ratio of

Hg (II) decreased with an increase in initial Hg (II) concentration where as the amount of Hg (II) uptake per unit weight of the adsorbent (mg/g) was found to increase, due to increased surface area, more adsorption sites are available causing higher removal of Hg (II), are shown in the table (2) and figure (1).

Batch experiments were carried out by varying the adsorbent dose between (20-4) g/L at the best initial concentration (10 mg/L) by change the weight of bentonite clay or change the volume of Hg (II) solution. The percentage of adsorption decreases from 88.7 to 68.9 and the adsorption capacity increases from 0.444 to 1.723 mg/g, are illustrated in the table (3). The increase in the percentage of adsorption is due to the increase in amount of free surface available or decreases the amount of Hg (II) in aqueous solution ⁽¹⁹⁾.

2- Influence of the shaken time:

Removal of mercury ion on the bentonite clay as a function of time at the best initial concentration (10 mg/L) was studied, where shaken it to different times between (20-200) min. From the experimental data, it is observed that the percentage of adsorption increased with increasing contact time up to 140 min. The percentage of adsorption increases from 61.3 to 88.7, because of the surface of bentonite clay contain oxygen atoms which bonded with mercury ion ⁽²⁰⁾, it is shown in the figure (2).

3- Effect of pH:

Adsorption experiments were performed over a range of pH (1-10) for the best initial mercury ion concentration (10 mg/L) and shaken time to 140 min. From figure (3) it is observed that the percentage of adsorption increase from pH (5-8). At low pH, i.e., higher hydrogen ion concentration, the negative charges at the surface of clay, become contend between H^+ ion and Hg (II) which bonded with oxygen atoms, it occur to decrease the percentage of adsorption. Above pH 8 the adsorption decrease, due to the effect of the hydroxyl ion, (Hg(OH)⁺) may be formed ⁽¹⁵⁾.

4- Effect of temperature:

Experiments were performed at different temperatures, from 288 to 328 K⁰ for the best initial mercury ion concentration (10 mg/L) at pH equal to 7 and shaken time to 140 min. The adsorption capacity of Hg (II) increased from 0.398 to 0.444 mg/g when the temperature increased from 288 to 328 K⁰, are shown in the table (4) and figure (4). The increase in the adsorption capacity showed the endothermic nature of the process.

The change in enthalpy (Δ H) and entropy (Δ S) were calculated from the plot of log (q_e/C_e) versus 1/T for mercury ion by using the Van't Hoff equation ⁽³⁸⁾, is shown in figure (5).

$\log \frac{q_e}{C} =$	$=\frac{\Delta S}{2.303R}$	$-\frac{\Delta H}{2.303RT}$	(3)
C_e Slope = -	$-\left(\frac{\Delta H}{2.303R}\right)$)	(4)
Intercept	$t = \left(\frac{\Delta S}{2.303}\right)$	\overline{BR}	(5)

The adsorption enthalpy of the mercury ion calculated from slope of the plot is 19.62 KJ/mol and entropy (Δ S) was also calculated from intercept of the plot is 94.163 J/mol.K⁰. These values of the heat of adsorption show that the type of adsorption onto bentonite clay is physical adsorption, because the adsorption with the heat that is lower than 20 KJ/mol⁽³⁵⁾. The change in free energy (Δ G) was calculated from Gibbs equation ⁽³⁶⁾:

The increase in the adsorption capacity of bentonite clay with temperature indicates an endothermic process. The positive value of (Δ S) suggested some structural changes in adsorbent and adsorbate and also reflects the affinity of the adsorbent material under consideration towards Hg (II) ions. The negative values of free energy (Δ G) show the spontaneous adsorption of metal ion on the adsorbent,

is illustrated in the table (5). The value of (ΔG) decreases with increasing temperature, demonstrating an increase in the feasibility of adsorption at higher temperatures.

5- Adsorption isotherm:

From the plot of q_e versus C_e of Hg (II) in figure (6), it is obvious that the adsorption isotherm of Hg (II) on bentonite clay is L-type according to the Gilles classification⁽³⁷⁾. In this type of isotherm, the initial portion provides information about the availability of the active site to the adsorbate and the plateau signifies the monolayer formation. The initial curvature indicates that a large amount of Hg (II) is adsorbed at a lower concentration as more active sites of bentonite clay are available. As the concentration increases, it becomes difficult for a Hg (II) ion to find vacant sites, and so monolayer formation occurs.

In order to determine isotherm model that described more accurately the experimental data, the model developed by Langmuir is represented by the following linear equation ⁽³⁸⁾:

$$\frac{C_e}{q_e} = \frac{1}{q_m b} + \frac{C_e}{q_m} \qquad \dots \dots (7)$$

Where q_e is the amount of adsorbate retained per unit weight of the adsorbent (mg/g) at equilibrium, C_e the equilibrium concentration of Hg(II) (mg/L), q_m and b are Langmuir constants related to the maximum saturation capacity of the bentonite clay (mg/g) and energy of adsorption (L/mg), respectively. The Langmuir constants (q_m and b) were calculated from the plots of C_e/q_e versus C_e , using linear least-squares fitting where the slope equal to ($1/q_m$) and the intercept equal to ($1/q_m b$). The values of the constants of this model with correlation coefficients (\mathbb{R}^2) are given in figure (7) and table (6).

6- Adsorption kinetic studies:

In the present studies, pseudo-first-order, pseudo-second-order equations have been used for modeling the kinetics of Hg(II) adsorption. The pseudo-first-order rate equation is expressed as:

$$\log(q_e - q_t) = \log q_e - \frac{\kappa_1 t}{2.303} \qquad \dots \dots (8)$$

Where q_t and q_e are the adsorption capacity at time, t, and at equilibrium, respectively, and k_1 is the rate constant of pseudo-first-order (min⁻¹) ⁽³⁹⁾. The values of k_1 at different adsorption parameters were calculated from the plot of log ($q_e - q_t$) as a function of the time for the best initial Hg(II) concentration (10 mg/L) at pH equal to 6 and temperature equal to 328 K⁰ should give a linear relationship where the slope equal to (- $k_1/2.303$) and the intercept equal to (log q_e), is given by figure (8) and table (7). Although the correlation coefficient values were higher than 0.99, the experimental q_e did not agree with the calculated q_e , obtained from the linear plots. Therefore, pseudo-first-order kinetic model did not describe the adsorption results of Hg(II) onto bentonite clay.

The pseudo-second-order rate equation is expressed as:

$$\frac{i}{q_t} = \frac{1}{(q_e)^2 k_2} + \frac{i}{q_e} \qquad \dots \dots (9)$$

Where k_2 is the rate constant of pseudo-second-order (g/mg.min), q_t and q_e are the adsorption capacity at time t and at equilibrium, respectively ⁽⁴⁰⁾. The values of k_2 were calculated from the plot of (t/q_t) versus (t) for the best initial Hg(II) concentration (10 mg/L) at pH equal to 6 and temperature equal to 328 K⁰, should give a linear relationship where the slope equal to (1/q_e) and the intercept equal to $[1/k_2.(q_e)^2]$, is given by figure (9) and table (8). It was noticed that the correlation coefficient value for the pseudo-second-order were found to be higher than that of the experimental q_e value. In the view of these results, it can be said that the pseudo-second-order kinetic model provided a good correlation for the adsorption of Hg(II) onto bentonite clay in contrast to the pseudo-first-order model.

Conclusion:

The bentonite clay was found to be a good adsorbent for the removal of Hg(II) ion from aqueous solutions. The Hg(II) ion removal efficiency of the adsorbent is found to be increase with the increase in time, temperature and adsorbent dose, when decrease with increase adsorbate concentration. The percentage adsorption increases with increasing temperature, which indicates that, the adsorption mechanism is endothermic. The experimental values were well fitted to the Langmuir isotherm equation, where found q_m and *b* are equal to 3.367 mg/g and 0.134 respectively. The adsorption kinetic followed a pseudo 2nd order rate equation where k_2 is equal to 0.1067 g/mg.min.

Table (1) Chemic	al analysis	of Bentonite	clay
	ai anaiysis	of Demonite	ciay

Oxides	$W_t \%$
SiO ₂	43.568
BaO	36.394
TiO ₂	9.245
Al_2O_3	6.321
CaO	2.655
MgO	1.368
Na ₂ O	0.449

Table (2). The effect of Hg(II) concentration on the percentage of adsorption and the adsorption capacity

C _i , mg/L	$C_e, mg/L$	% Adsorption	$q_e, mg/g$
100	42.6	57.4	2.87
90	34.74	61.4	2.763
80	26.8	66.5	2.66
70	20.93	70.1	2.454
60	15.42	74.3	2.229
50	10.35	79.3	1.983
40	7.12	82.2	1.644
30	4.56	84.8	1.272
20	2.56	87.2	0.872
10	1.13	88.7	0.444

Table (3). The effect of the adsorbent dose on the percentage of ada	sorption and the adsorption
capacity for the best initial concentration (10	mg/L)

m, g	V, L	adsorbent dose, g/L	C _e , mg/L	% Adsorption	q _e , mg/g
0.5	0.025	20	1.13	88.7	0.444
0.4	0.025	16	1.84	81.6	0.51
0.3	0.025	12	2.08	79.2	0.66
0.5	0.05	10	2.24	77.6	0.776
0.2	0.025	8	2.67	73.3	0.916
0.5	0.1	5	2.98	70.2	1.404
0.1	0.025	4	3.11	68.9	1.723

Table (4). The effect of temperature on the adsorption capacity $\frac{1}{1}$

K^0	$1/K^{0}$	C _e , mg/L	q _e , mg/g	$\log q_e/C_e$
288	0.00347	2.04	0.398	-0.710
298	0.00335	1.82	0.409	-0.648
308	0.00324	1.57	0.422	-0.571
318	0.00314	1.30	0.435	-0.475
328	0.00304	1.13	0.444	-0.406

K^0	$1/K^{0}$	Δ H, KJ/mol	$\Delta S, J/mol.K^0$	$\Delta G, KJ/mol$	% Adsorption
288	0.00347			-1.516	79.6
298	0.00335			-2.053	81.8
308	0.00324	13.924	53.614	-2.589	84.3
318	0.00314			-3.125	87
328	0.00304			-3.661	88.7

Table (5). The calculate the thermodynamic parameters and effect on the adsorption ratio

Table (6). Langmuir isotherm parameters

q _m , mg/g	b	\mathbf{R}^2
3.367	0.134	0.9998

Table (7). Pseudo-first-order kinetic constants for adsorption Hg(II) on kaolinite clay

q _e , _{exp.} mg/g	q _e , _{cal.} Mg/g	$k_1 (min^{-1})$	\mathbf{R}^2
0.444	0.2447	0.082	0.9342

Table (8). Pseudo-second-order kinetic constants for adsorption Hg(II) on kaolinite clay

$q_{e, exp.} mg/g$	q _e , _{cal.} mg/g	k ₂ (g/mg.min)	R^2
0.444	0.4867	0.1067	0.9959



Figure (1). The effect of initial Hg(II) concentration on the percentage of adsorption



Figure (2). The effect of shaken time on the percentage of adsorption



Figure (3). The effect of pH on the percentage of adsorption



Figure (4). The effect of temperature on the adsorption capacity







Figure (6). The adsorption isotherm of Hg(II) on bentonite clay



Figure (7). Linear form of Langmuir equation for adsorption Hg(II) on bentonite clay



Figure (8). Pseudo-first-order kinetic for adsorption Hg(II) on bentonite clay



Figure (9). Pseudo-second-order kinetic for adsorption Hg(II) on bentonite clay

References:

1. C. Baird, **Environmental Chemistry**, W.H. Freeman and Company, New York, U.S.A., (1995), P. 3.

2. D. G. Crosby, **Environmental Toxicology and Chemistry**, Oxford University Press, New York, U.S.A., (1998), P.112.

3. N.N. Greenwood and A. Aernshaw, **Chemistry of the Elements**, 2nd Edition. Oxford Butterworth Heinemann, New York, U.S.A., (1997), P.93.

4. J. Alloway and D.C. Ayres, **Chemical Principles of Environmental Pollution**, Chapman and Hall, Oxford, New York, U.S.A., (1993), P.64.

5. P. Englezos and N. Kalogerakis, **Applied Parameter Estimation for Chemical Engineers**, Marcel Deccer, Inc., New York, U.S.A., (2001), P.78.

6. J. C. Hower, M. M. Valer, D. N. Taulbee and T. Sakulpitakphon, **Mercury**, Oxford University Press, New York, U.S.A., (2000), P.224.

7. R. Petrus and J. Warchol, Mesopor. Mater., 61, (2003), P.137.

8. M. Khraished, Y. Al-degs and W. Mcmin, Chem. Eng. J., 99, (2004), P.177.

9. A. Dabrowski, Z. Hubicki, P. Podkoscielny and E. Robens, Chemosphere, 56, (2004), P.91.

10. E. K. Yetimoglu, M. V. Kahraman, O. Ercan, Z. S. Akdemir and N. K. Apohan, **React. Funct. Polym.**, 67, (2007), P.451.

- 11. H. A. Essawy and H.S. Ibrahim, React. Funct. Polym., 61, (2004), P.421.
- 12. F. S. Zhang, J. O. Nriagu and H. Itoh, J. Photochem. Photobiol. A Chem., 167, (2004), P.223.
- 13. C. C. Wang, C. Y.Chen and C. Y. Chang, J. Appl. Polym. Sci., 84, (2002), P.1353.
- 14. G. Skodras, I. Diamantopoulou, G. Pantoleontos and G.P. Sakellaropoulos, J. of Hazar. Mater., 158, (2008), P.1.
- 15. Y. S. Ho and C. C. Wang, J. of Hazar. Mater., 156, (2008), P.398.
- 16. K.G. Bhattacharyya and S.S. Gupta, Colloids Surf., 277, (2006), P.191.
- 17. S. S. M. Hassan, N. S. Awwad and A. H. A. Aboterika, J. of Hazar. Mater., 154, (2008), P.992.
- 18. J. B. Patel and P. Sudhakar, EJEAFChe., 7, (2008), P.2735.
- 19. S. S. Tahir and R. Naseem, Sep. Purif. Technol., 53, (2007), P.312.
- 20. E. Eren and B. Afsin, J. of Hazard. Mater., 151, (2008), P.682.
- 21. Z. Rawajfih and N. Nsour, J. Colloid Interf. Sci., 298, (2006), P.39.
- 22. S. Andini, R. Cioffi, F. Montagnaro, F. Pisciotta and L. Santoro, Appl. Clay Sci., 31, (2006), P.126.
- 23. M. Akcay and G. Akcay, J. of Hazard. Mater., 113, (2004), P.189.
- 24. F. Ayari, E. Srasra and M. T. Ayadi, Desalination, 206, (2007), P.499.
- 25. A. Demirbas, A. Sari and O. Isildak, J. of Hazard. Mater., 135, (2006), P.226

26. M. Bacquet, B. Martel, M. Morcellet, K. I. Benabadji, K. Medjahed, A. Mansri, A. H. Meniai and M. B. Lehocine, **Mater. Lett.**, 58, (2004), P.455.

- 27. T. Asselman and G. Garnier, Colloids Surf. A, 168, (2000), P.175.
- 28. E. Bojemueller, A. Nennemann and G. Lagaly, Appl. Clay Sci., 18, (2001), P.277.
- 29. J. Bors, S. Dultz and B. Riebe, Appl. Clay Sci., 16, (2000), P.1.
- 30. Q. Y. Yue, Q. Li, B. Y. Gao and Y. Wang, Sep. Purif. Technol., 54, (2007), P.279.
- 31. E. Eren and B. Afsin, Dyes Pigments, 76, (2008), P.220.

32. H. H. Murray, Applied Clay Mineralogy Occurrences, Processing and Application of Kaolins, Bentonites, Palygorskite, Sepiolite, and Common Clays, Elsevier, Amsterdam, The Netherlands, (2007), P.111.

- 33. G. H. Hu and F. Haghseresht; ARC Center for Functional Nanomaterials, 2, (2001), P.19.
- 34. R. Lobinski and Z. Marcozenko, **Spectrochemical Trace Analysis For Metals And Metalloids**, Elsevier, New York, U.S.A., (1990), P.520.

35. W.G. Castellan, **Physical Chemistry**, 3rd edition, The Benjamin Cummings Publishing Company, Inc., California, U.S.A., (1982), P.428.

36. P. Atkins and J.D. Paula, Atkins' Physical Chemistry, 8th edition, Oxford University Press, New York, U.S.A., (2006), P.100.

37. C.H. Gilles, T.H. Macewan, S.N. Nakhwa and D. smith, J. Chem. Soc., 10, (1960), P.3973.

38. I. Langmuir, J. Am. Chem. Soc., 38, (1916), P. 2221

39. B.A. Cemioglu, Chem. Eng. J., 106, (2005), P. 73.

40. M.X. Loukidous, A.I. Zouboulis, T.D. Karapantsios and A. Martis, Colloid Surf. Phys. Chem. Eng. Aspects, 242, (2004) P. 93.