

$$\begin{aligned}
 & \text{The relationship between the contraction ratio } (B_1/B_2) \text{ and the depth of scour } (d_s) \text{ is given by:} \\
 & d_s = 0.0001 (B_1/B_2)^{2.151} (Fr_o)^{0.474} (\sigma_g)^{0.9343} \\
 & \text{where } (Fr_o) \text{ is the densimetric particle Froude number and } (\sigma_g) \text{ is the geometric standard deviation.} \\
 & \text{The correlation coefficient } (R^2 = 0.9434) \text{ indicates a strong linear direct relation.}
 \end{aligned}$$

### LABORATORY STUDY OF SCOUR IN LONG CONTRACTIONS

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#### ABSTRACT

In this investigation, scour in long contractions phenomenon was studied experimentally. For this purpose, forty laboratory experiments were carried out in a laboratory channel. Two different river sand sizes of 0.653 mm, 1.040 mm were used to conduct the experiments with standard deviations of 2.151 and 3.474 respectively. Three different ratios of contraction ( $B_1/B_2 = 4, 3$  and 2) and three different angles of contraction ( $\theta = 10, 15$  and 20 degrees) were tested. For each case, the discharge was changed four times from 10.4 Liter/sec to 47.6 Liter/sec.

Data analysis showed that depth of scour ( $d_s$ ) depends mainly on contraction ratio ( $B_1/B_2$ ), densimetric particle Froude number ( $Fr_o$ ) and geometric standard deviation ( $\sigma_g$ ). Results of this study showed that there is a strong linear direct relation between the ratio of the contraction channel width and the depth of scour. Also a direct relationship was found to describe the effect of discharge on depth of scour. The results showed that there is no effect of contraction angle on the scour depth in long contractions. Also, an empirical non-dimensional relationship was obtained to determine depth ratio ( $Y_2/Y_1$ ) in long contraction with correlation coefficient ( $R^2 = 0.9343$ ).

The results of the present investigation were compared with those of other investigators showing a good agreement among them.

$\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{\frac{6}{7}} \left[ \frac{\tau_c}{2\tau_1} + \sqrt{\left(\frac{\tau_c}{2\tau_1}\right)^2 + \left(1 - \frac{\tau_c}{\tau_1}\right)\frac{B_1}{B_2}} \right]^{\frac{-3}{7}}$  .....(1)  
 (Komura,1966) (1)  $\left(1 \leq \frac{L}{B_1}\right)$   
 (è)

(Straub,1934) (1940-1934)  
 $\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{\frac{9}{14}}$  .....(2)  
 (Griffith,1939)

(Laursen,1958b) (è)  
 $\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{\frac{6(2+a)}{7(3+a)}} \times \left(\frac{n_2}{n_1}\right)^{\frac{6(a)}{7(a+3)}}$  .....(i)  
 (ω) (V\*)  
 $1/4 = a$   $1/2 > V^*/\omega$

(è)  
 $\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{\frac{9}{14}}$  .....(2)  
 (Griffith,1939)

$$\frac{U_2}{U_1} = \left( \frac{B_1}{B_2} \right)^{0.593} \quad (n_2 = n_1) \quad (4)$$

$$\frac{Y_2}{Y_1} = \left( \frac{B_1}{B_2} \right)^{0.593} \quad (\hat{e}, \hat{e}i = a) \dots\dots\dots (5)$$

$$\frac{Y_2}{Y_1} = \left( \frac{B_1}{B_2} \right)^{0.694} \quad (\hat{e}, \hat{e}i = a) \dots\dots\dots (6)$$

Laursen,1963

$$\tau_o' = 17.2 \frac{v_1^2 D_{50}^{\frac{1}{3}}}{y_1^{\frac{1}{3}}} \dots\dots\dots (7)$$

$$\tau_c = 0.628 \times D_{50} \dots\dots\dots (8)$$

$$\frac{Y_2}{Y_1} = \frac{ds}{Y_1} + 1 = \left( \frac{\tau_o'}{\tau_c} \right)^{\frac{3}{7}} \times \left( \frac{B_1}{B_2} \right)^{\frac{6}{7}} \dots\dots\dots (9)$$

(Komura,1966)

$$\frac{Y_2}{Y_1} = 1.45 \times (Fr_1)^{\frac{1}{5}} \times \left( \frac{B_1}{B_2} \right)^{\frac{2}{3}} \times (\sigma_g)^{\frac{-1}{5}} \dots\dots\dots (10)$$

(Froude number)

$$\frac{Y_2}{Y_1} = 1.60 \times (Fr_1)^{\frac{1}{5}} \times \left( \frac{B_1}{B_2} \right)^{\frac{2}{3}} \times (\sigma_g)^{\frac{1}{2}} \dots\dots\dots (11)$$

Laursen and ) (Silverstone,1976

(K<sub>1</sub>/K<sub>2</sub>) (k<sub>2</sub>/k<sub>1</sub>)

$$\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{\frac{6(a+2)}{7(a+3)}} \times \left(\frac{n_2}{n_1}\right)^{\frac{6a}{7(a+3)}} \times \left(\frac{k_2}{k_1}\right)^{\frac{6}{7(a+3)}} \times \left(\frac{K_1}{K_2}\right)^{\frac{a}{a+3}} \dots\dots\dots(1\hat{e})$$

(Alawi,1981)  
 (Alawi,1985)  
 (Y<sub>2</sub>/Y<sub>1</sub>)  
 (V\*/ω)  
 (m) (é) (Gill,1981) Û

$$\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{\frac{6}{7}} \times \left[ \frac{\tau_c}{\tau_1} + \left(1 - \frac{\tau_c}{\tau_1}\right) \times \left(\frac{B_1}{B_2}\right)^{\frac{1}{m}} \right]^{\frac{-3}{7}} \dots\dots\dots(é\grave{e})$$

(é\grave{e}) (τ<sub>1</sub> = τ<sub>o</sub>') (τ<sub>1</sub> ≤ 1)  
 (τ<sub>c</sub> → 0) (ñ)  
 (m=1.5) (m=3)  
 (é\grave{e}) Û Û

$$\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{0.714} \dots\dots\dots(14)$$

$$\frac{Y_2}{Y_1} = \left(\frac{B_1}{B_2}\right)^{0.571} \dots\dots\dots(15)$$

(é) (é\grave{e}) (m=0.25) Û  
 (Lim and Cheng,1998)

$$\left(\frac{Y_2}{Y_1}\right) = \left(\frac{B_1}{B_2}\right)^{0.75} \dots\dots\dots(16)$$

∅ (é)

$$Y_2 = f(Y_1, B_1, B_2, v_1, g, D_{50}, \rho_w, \Delta\rho_s, \mu, \theta, \sigma_g) \dots\dots\dots(17)$$

$$\frac{Y_2}{Y_1} = f\left(\frac{B_1}{B_2}, Fr_o, \sigma_g, \theta, Re\right) \dots\dots\dots(18)$$

$$\left( \frac{v_1}{\sqrt{g \frac{\Delta \rho_s}{\rho_w} D_{50}}} \right) = Fr_o$$

$$\left( \frac{v_1 Y_1 \rho_w}{\mu} \right) = Re$$

$$\rho_s - \rho_w (= \Delta \rho_s)$$

:

$$ds = Y_2 - Y_1 + \frac{v_2^2}{2g} - \frac{v_1^2}{2g} + H_L \dots\dots\dots(19)$$

:

$$\left( \quad \right) = \frac{v_1^2}{2g}$$

$$\left( \quad \right) = \frac{v_2^2}{2g}$$

$$= H_L$$

: (19)

$$ds = Y_2 - Y_1 \dots\dots\dots(20)$$

-: Ø (ë)

( 1.25 × 2.25 ) ( 15.24 ) ( 0.3 ) ( 0.81 × 3.0 ) ( 0.5 ) ( 1.0 × 0.5 )  
 ( 0.81 ) ( 1.2 ) ( 8 ) ( 0.5 ) ( 1.84 ) ( 0.6 ) ( 49.6 × 17 ) ( 1.75 ) ( 0.6 )



( / )	( 0.653 = D <sub>50</sub> ) A			( 1.04 = D <sub>50</sub> ) B		
	a <sub>1</sub>	b <sub>1</sub>	R <sup>2</sup>	a <sub>1</sub>	b <sub>1</sub>	R <sup>2</sup>
47.573	-3.3500	5.440	0.9997	-6.0683	5.225	0.9816
36.271	-3.1467	4.250	0.9948	-9.6433	5.020	0.9998
22.676	-2.7500	2.890	0.9624	-5.8533	2.940	0.7500
10.398	-1.3367	1.250	0.9979	-2.4617	1.055	

$$ds = a_2 + b_2 \times Q \dots\dots\dots(22)$$

$$\frac{ds}{dQ} = b_2 = a_2$$

$$\frac{ds}{dQ} = Q$$

$$\frac{ds}{dQ} = (b_2, a_2)$$

الحالة	النموذج A (0.653 = D <sub>50</sub> ملم)			النموذج B (1.04 = D <sub>50</sub> ملم)		
B <sub>1</sub> /B <sub>2</sub>	a <sub>2</sub>	b <sub>2</sub>	R <sup>2</sup>	a <sub>2</sub>	b <sub>2</sub>	R <sup>2</sup>
4	-0.0033	0.3708	0.9786	-2.1182	0.3420	0.9828

$$\frac{\tau_o'}{\tau_c} = 0.02739 \times \left( \frac{v_1^2}{Y_1 \frac{1}{3} D_{50} \frac{2}{3}} \right) \dots\dots\dots(23)$$

(Laursen) 
$$\left( \frac{\tau_o'}{\tau_c} \right)_L = \dots\dots\dots$$

$$\frac{\tau_o'}{\tau_c} = a_3 + b_3 \times \left( \frac{Y_2}{Y_1} \right) \dots \dots \dots (24)$$

(24)      (R<sup>2</sup>)      Ø      (b<sub>3</sub>, a<sub>3</sub>)      (4) Ø

(24)		(R <sup>2</sup> )			(4) Ø		
		( 0.653 = D <sub>50</sub> ) A			( 1.04 = D <sub>50</sub> ) B		
B <sub>1</sub> /B <sub>2</sub>	θ°	a <sub>3</sub>	b <sub>3</sub>	R <sup>2</sup>	a <sub>3</sub>	b <sub>3</sub>	R <sup>2</sup>
4	20	-1.2281	1.6223	0.9853	-1.0241	1.6449	0.9858
3	20	-1.3944	1.4904	0.9958	-1.0233	1.3366	0.9854
2	20	-1.2651	1.1905	0.9979	-1.0243	1.1552	0.9856

$$\frac{Y_2}{Y_1} = 0.618 \times \left( \frac{B_1}{B_2} \right)^{0.527} \times (Fr_o)^{0.489} \dots \dots \dots (25)$$

(25)      (R<sup>2</sup>)      Ø      (b<sub>3</sub>, a<sub>3</sub>)      (4) Ø

$$\frac{Y_2}{Y_1} = 0.618 \times \left( \frac{B_1}{B_2} \right)^{0.527} \times (Fr_o)^{0.489} \dots \dots \dots (25)$$

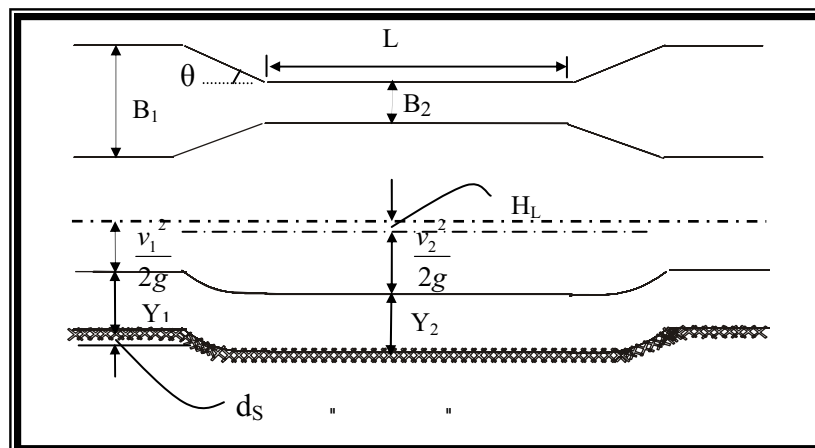
(25)      (R<sup>2</sup>)      Ø      (b<sub>3</sub>, a<sub>3</sub>)      (4) Ø



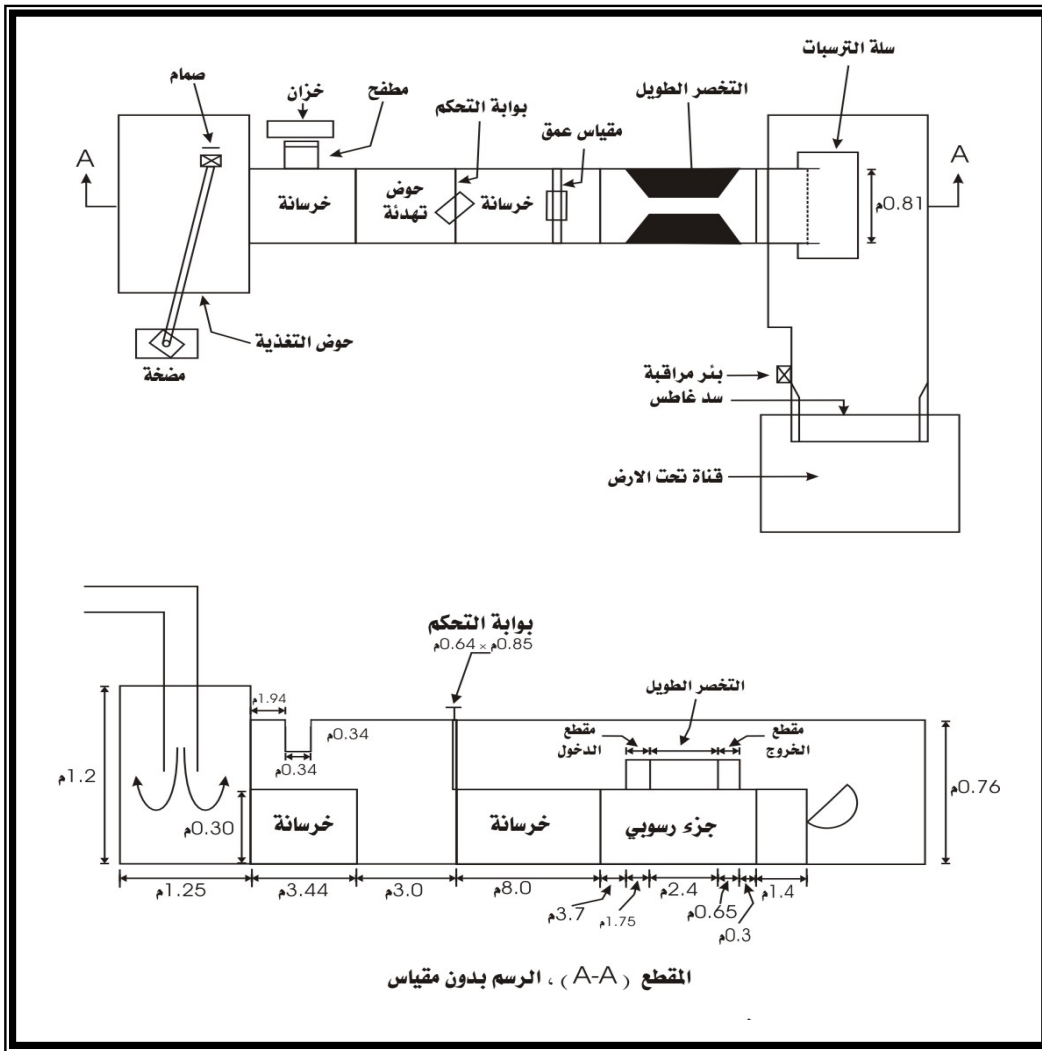


(i)

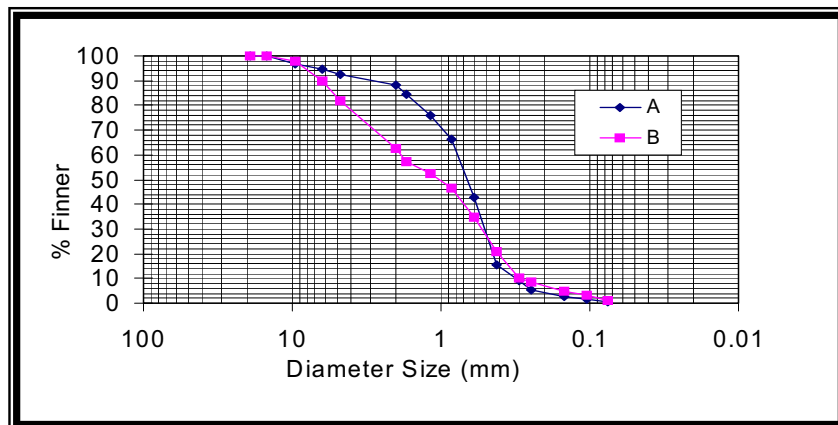
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Ø : (1) Ø

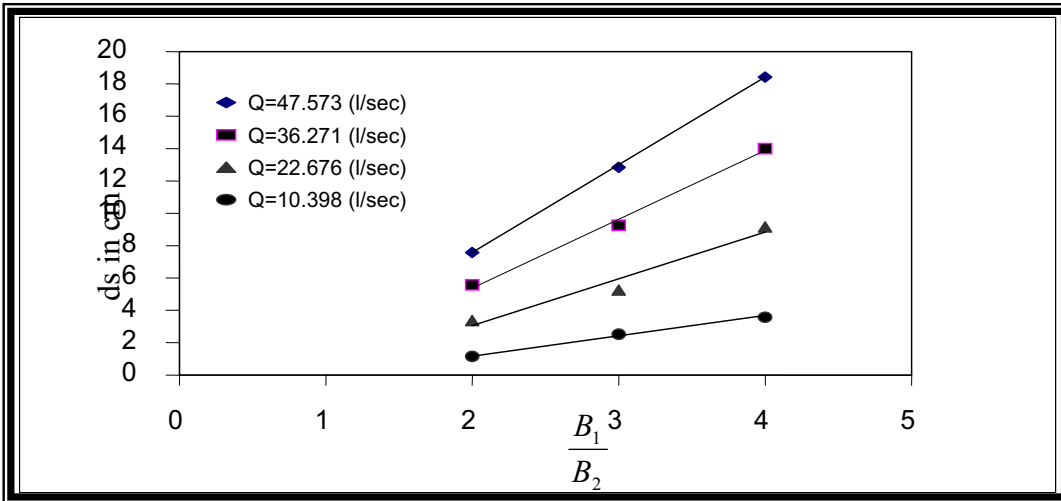


: (é) Ø

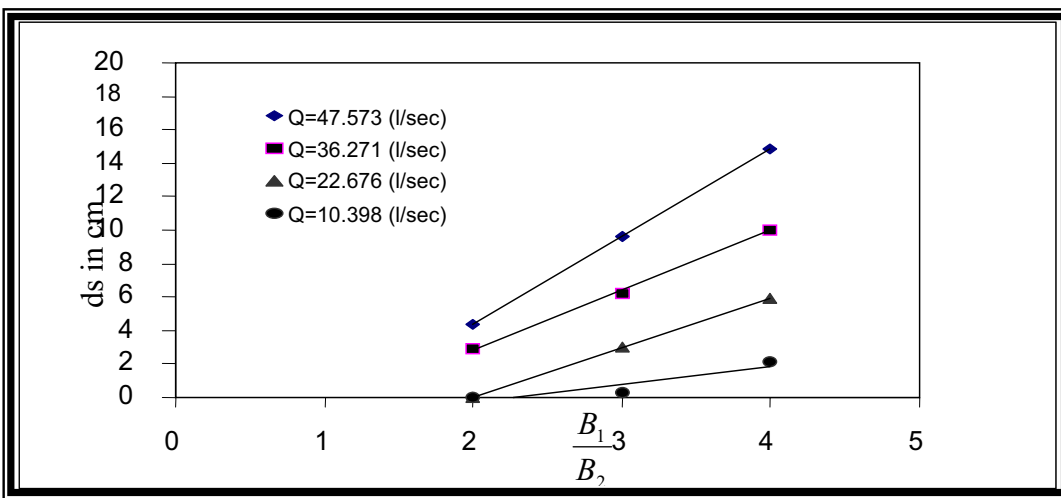


Ø

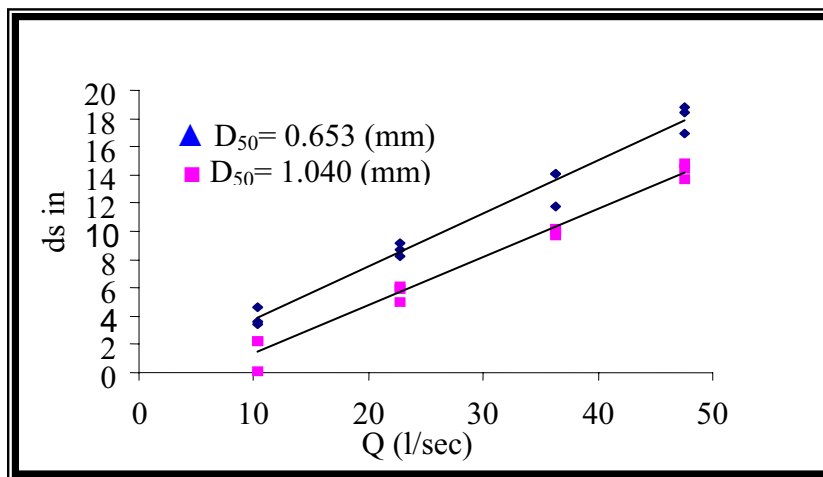
: (é) Ø



شكل (4) : العلاقة بين عمق النحر ونسبة التخصر للنموذج A

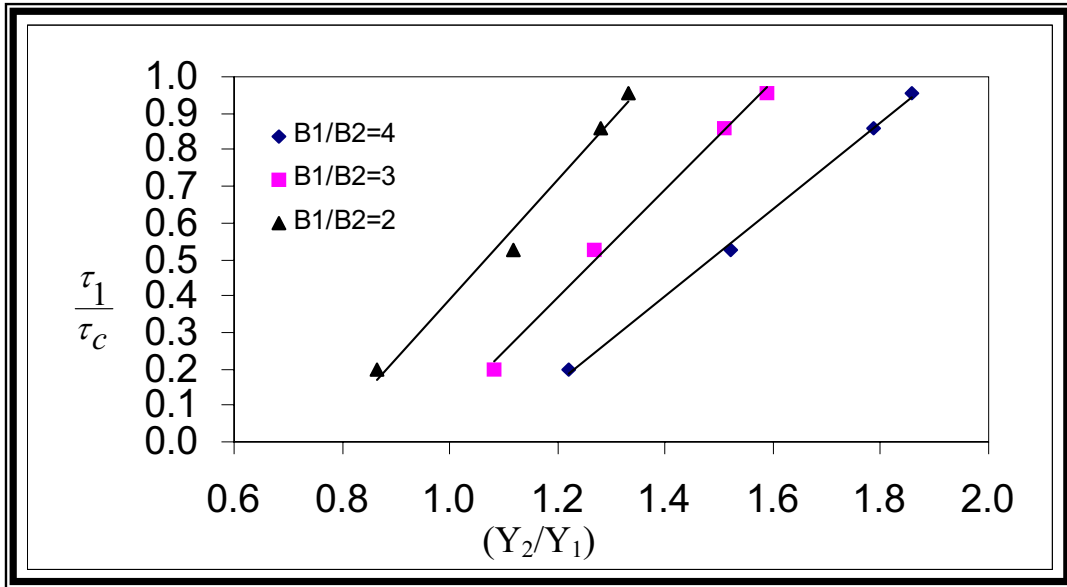


شكل (5) : العلاقة بين عمق النحر ونسبة التخصر للنموذج B



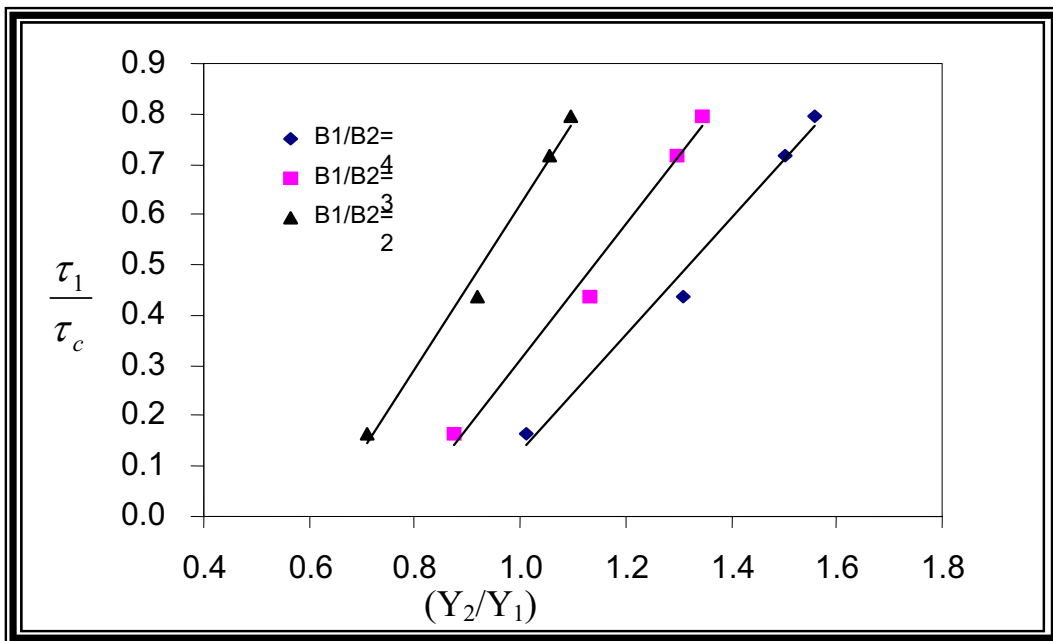
( $\theta=10^\circ, 15^\circ, 20^\circ$ ) ( $B_1/B_2=4$ )

(i)  $\emptyset$



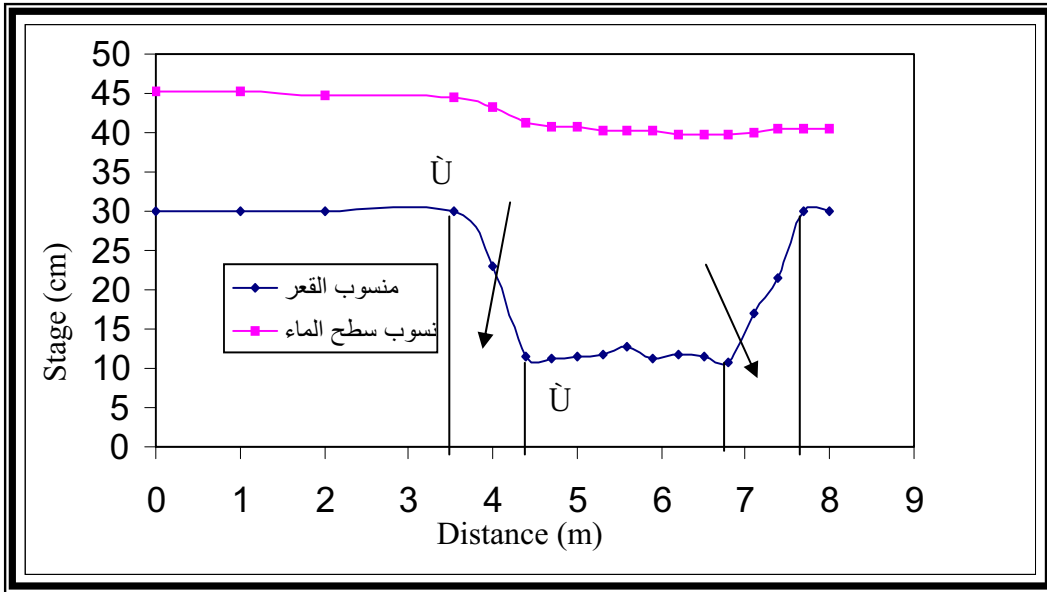
A

(i) Ø



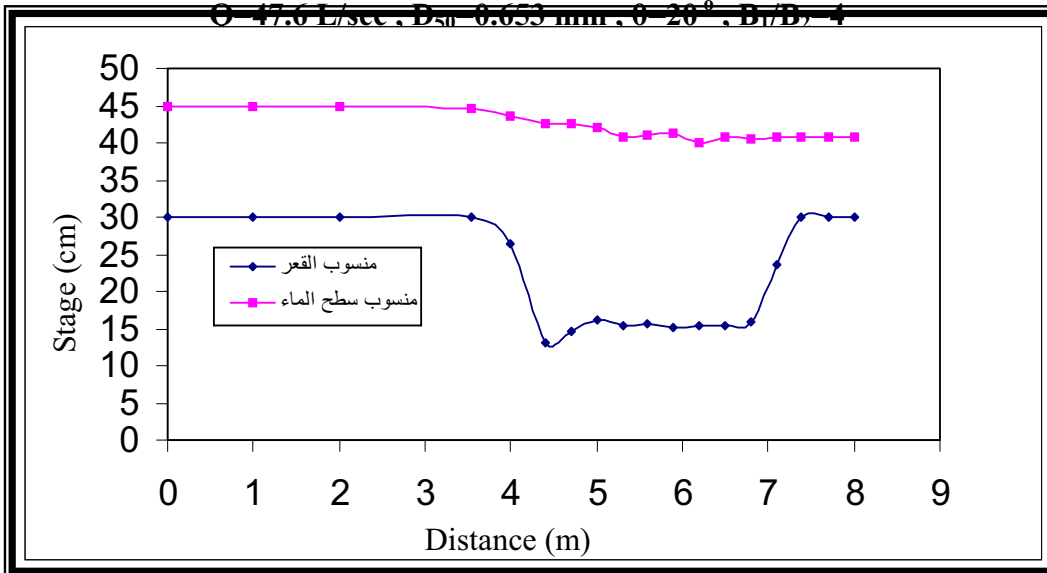
B

(i) Ø



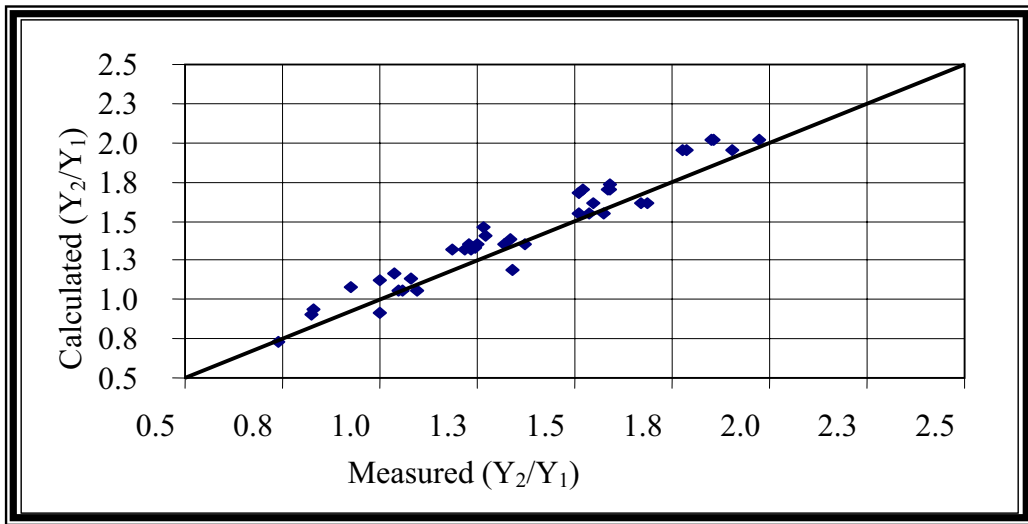
A Ø : (ø) Ø

Q=47.6 L/sec, D<sub>50</sub>=0.653 mm, θ=20°, B<sub>1</sub>/B<sub>2</sub>=4

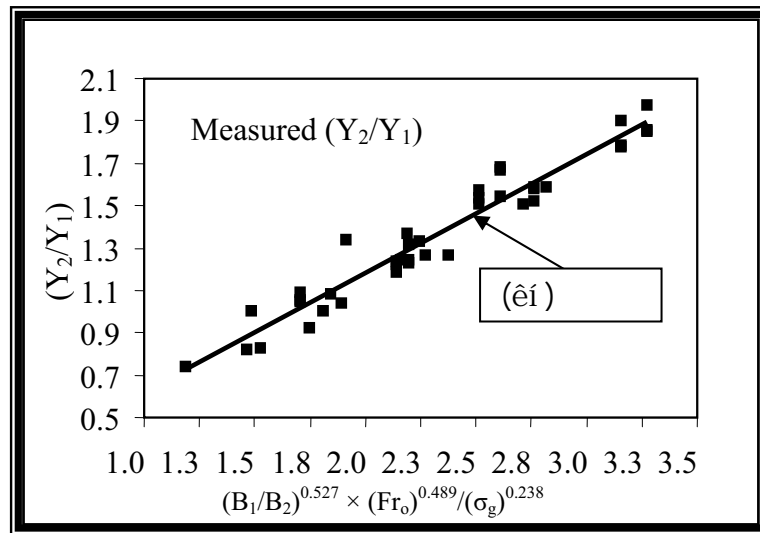


B Ø : (èç) Ø

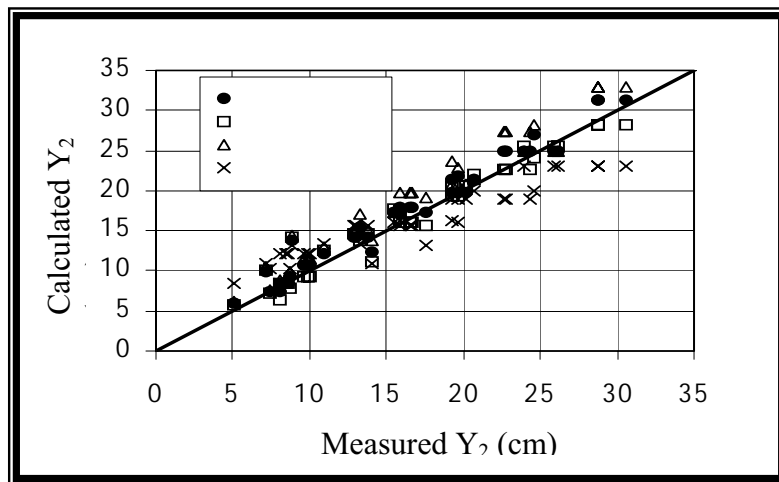
Q=47.6 L/sec, D<sub>50</sub>=0.1.04 mm, θ=20°, B<sub>1</sub>/B<sub>2</sub>=4



(èì) : (èè) Ø



(èì) : (12) Ø



: (13) Ø