

(2004/6/22 2003/10/20 )

.( )

(Electrical sounding)

.(GMS)

( 10<sup>9</sup> x21)

(10<sup>9</sup>x 136 )

## **Using GMS to Formulate the Geological Sections for Hamdania Region, North Iraq**

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### **ABSTRACT**

Predicting Three dimation solid model for aquifers in any region is one of the most important aims for hydrologists to reach. The Electrical investigation data have been used

for Hamdania region. This data represent the aquifers thickness in electrical sounding points. A Three dimension computerized solid model was build using the groundwater modeling system (GMS). This has been done by connecting the aquifer upper points to make triangular irregular network (TIN), which is repeated for all aquifers in the study region to make four TINs. By filling between these TINs a 3D solid model was build for geological aquifers in the study region. The size and the dimentions for all aquifers were calculated from this model. The volume for Bi Hasan Formation is  $(21 \times 10^9) \text{ m}^3$  while the volume for Injanah Formation is  $(136 \times 10^9) \text{ m}^3$ .

(GMS)

(Groundwater Modeling System)

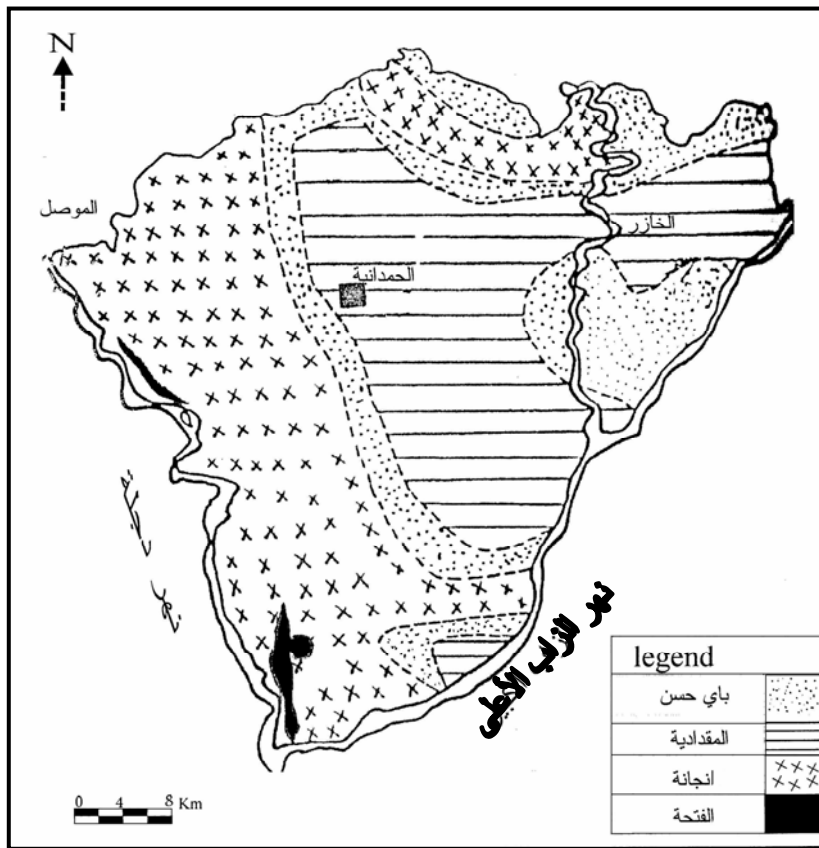
( 35)

(  $43^\circ 32'00'' - 43^\circ 10' 00''$  )

(  $36^\circ 00' - 36^\circ 20' 30''$  )

<sup>2</sup> (950)

.(1 )



:1

(2000 )

(Quaternary) (Tertiary)  
 :(1988 ) (1977 )

:( )

.(Al-Mubarak and Yokhanna, 1977)

:( )

.(2000 ) (200)

:( )

:( )

) :

(

.(Al-Dabagh, and Al-Naqib, 1991)

GMS

,

.(2000 )

( 1 )

(Schlumberger)

.(ABEM SAS 300)

AB=1500

.(Griffiths and King , 1981) ,

(1 )

(2 )

(Groundwater Modeling System) (GMS)

.(Finite Elements)

(1 )

)

(41)

(3

				( )			
P1	29100	45800	324	6	14	168	26
P3	33000	43400	310	7	3	190	60
P4	20400	47000	290	10	0	80	30
P6	19200	44300	290	8	4	108	20
P7	25300	43500	300	8	24	168	40
P8	29150	41450	304	12	8	140	30
P9	35550	38400	280	8	10	78	26
P10	34900	34100	292	3	29	68	35
P12	26400	38900	308	8	12	140	28
P13	21400	42750	280	10	12	140	22
P14	12850	42350	268	9	12	149	40
P15	17300	40500	270	10	10	148	30
P16	24700	36800	280	10	0	110	20
P17	29850	33550	300	8	9	123	35
P18	32900	32150	300	5	8	117	18
P19	30200	30100	288	2	18	140	22
P21	21500	35300	280	10	5	135	25
P22	20550	34600	280	10	12	70	32
P23	14550	37800	300	8	12	140	28
P24	8400	39800	250	8	0	88	8
P25	16700	34800	280	9	1	87	10
P27	31700	26650	260	8	18	58	34
P28	26800	26650	260	4	22	134	30
P30	8000	35100	260	12	0	22	2
P31	2500	37700	214	6	0	26	6
P32	4250	32900	235	5	0	12	0
P33	10650	31300	260	4	2	68	4
P35	23100	26450	260	6	54	112	72
P35	27750	22600	246	6	34	68	46
P37	34600	20250	260	4	16	214	24
P38	33550	15150	242	9	2	189	20
P39	17900	24050	274	10	0	130	20
P42	16750	21600	260	2	6	72	10
P43	21100	19600	256	5	35	160	45
P44	25300	16400	228	8	12	52	28
P46	31200	8900	250	10	4	170	24
P48	12600	20000	198	5	0	20	4
P49	16350	13450	196	2	26	92	70
P50	29600	6500	224	6	14	140	26
P52	17950	5700	218	2	8	120	22
P53	25450	3200	200	2	0	154	31

:2

.(2000 )

( )

( )

.( )

.(4)

. : 3

: 4

(Extrapolation)

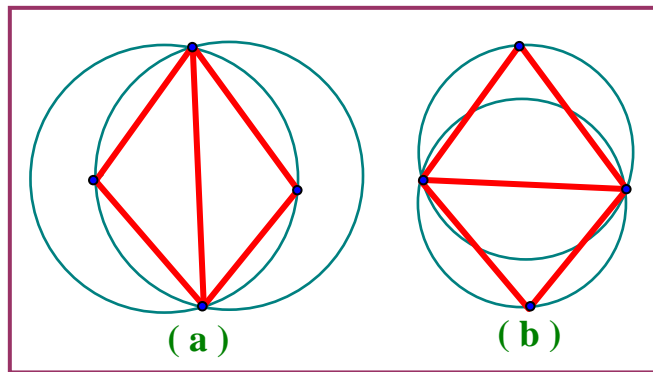
(Delauney)

(a)

(5 )

(b)

(GMS, 1996)



(a)

Delauney

:5

(b)

(6 )

(7 )

( )



:6

:7

:

$$\begin{aligned}
 & \cdot \\
 & \quad (20-) \\
 & \quad ) \cdot (8 \quad ) \\
 & \quad \quad \cdot (
 \end{aligned}$$

:

$$\begin{aligned}
 & \quad \cdot \\
 & \quad \quad (136 \times 10^9) \\
 & \quad \quad \cdot (9 \quad )
 \end{aligned}$$

:

$$( \quad \quad \quad )$$

$$\cdot (9 \quad )$$

$$\cdot \quad (10^9 \times 21)$$

$$\cdot \quad (10^9 \times 9.7)$$

$$\cdot (9 \quad )$$

:8

:9

(12) .(10 )  
(11)

(Y)

(11 )

(12 )

( )

(Z)

( Y)

(X)

(Z)

(X)

( )

:10

:11



.1988

133

.1977

199

.2000

126.

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