

Analysis and Design of 460 GHz Microwave Gyrotron Oscillator

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K E Y W O R D S	ABSTRACT	
Gyrotron, microwave tubes, millimeter-wave source, high-frequency device.	This paper is concerned with the an oscillator with 460 GHz that can fundamental (230GHz) and (TE061, 460GHz). The oscillator is operated with beam current, and a computer program in this oscillator and the wave-partice forward finite difference technique as a of the program are electron energy, length, the normalized value of the en number (m,n,l), and nth-non van shinin, the beam and starting currents, frequent The results show good agreement with [13]- [14], [15]. This oscillator can ser the magnetic field of (16.4T) for enhan- and can be used to perform the biological	alysis and design of a gyrotron excite both modes (TE231) the TE261) second harmonic (near th 12KV beam voltage and 100mA was developed to study the cavity le interaction inside it using the numerical method. The input data velocity ratio, normalized cavity xternal magnetic field, the mode g root of $J_m^{\wedge r}(x)=0$ to calculate cy and quality factor of the cavity. other reported works [10]- [12]- we as a millimeter-wave source at nced nuclear magnetic resonance al experiment.

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1. INTRODUCTION

The electromagnetic spectrum between (300-3000GHz), is interested in Radar applications in Communications, and spectroscopy [1]-[2],[3]. At frequencies (100-170GHz) plasma heating for fusion application. The region of interaction with the electron beam in microwave devices necessarily scales with the wavelength, the increasing frequency of these devices utility above 140GHz. The operating wavelength is smaller than the physical dimensions of the resonator [4]. The highest frequency is 889GHz at Fukui University in Japan [5]. The second harmonic operation of a soviet gyrotron frequency is 326GHz with a power of 1.5 kW [6]. To elevated ohm losses depending on the fundamental interaction to get high efficiency. To operation at higher harmonics interaction needs a

large magnetic field. It requires a stronger field for efficient interaction between the beam and the wave. It suffers from the additional complication of mode competition. Efficient interaction between the beam and the wave takes place when the distance between the beam and the surface of the wave guide or cavity structure is smaller than the wave length, this gives rise to increase power loss due to wall heating, which leads to decrease of output microwave power [9]. Furthermore, ohmic loss is a limiting factor in the design of high Q cavities, which is necessary to lower starting current to the operating range of the low power electron gun. In this work when the distance between the beam and the surface of the wave guide or cavity is smaller than the wave length, the power loss increase due to wall heating, which leads to a decrease of output microwave power [7].

2. METHODOLOGY

In this study, a single open-cavity configuration in which an annular mono energetic electron beams sustaining a constant amplitude normal mode of oscillation is considered, the electron emitted by the magnetron injection gun move with a helical path interacting with the wave in the cavity, the electron beam gathers on the collector. The basic schematic of gyrotron is shown in Figure (1.b). The simple cavity of gyrotron operates at 1.5 Mw or below output power. In the gyrotron. In Figure (1.a) the electron beams gyrating with a cyclotron frequency near the operating frequency of the device around and in the magnetic field [8, 9].



Figure 1: (a) Single cavity of the gyrotron [10], (b) The gyrotron cavity

The beam electrons propagate in an annulus with a constant radius of guiding center (Rg), space charge fields of the beam are neglected i.e no field emission and axial-symmetric TE – modes are exited. Under these circumstances, the relativistic electron Equation of motion is a combined electric field E and the magnetic field B is:

$$\frac{\partial}{\partial t}[mv(r, \emptyset, z, t)] = -e[E_{(r, \emptyset, z, t)} + v_{(r, \emptyset, z, t)} \times B_{(r, \emptyset, z, t)}]$$
(1)
Where $v(r, \phi, z, t)$ is th

e electron velocity, *e*, and *m* are the electron charge and relativistic mass respectively. $m = \gamma_{ral} m_o$: m_o is the electron rest mass and γ is the relativistic factor

$$\gamma_{ral} = \left[1 - \frac{v^2}{c^2}\right]^{-\frac{1}{2}}$$
Where *C* is the speed of light. (2)

The components of Equation (1) in cylindrical coordinates are:

$$\frac{\partial}{\partial t}(mr) - \frac{m\theta}{r} = -e(E_r + r\theta B_z - z B_\theta)$$
(3a)

$$\frac{\partial}{\partial t}(m\theta) - \frac{r\cdot\theta}{r} = -e(E_{\theta} + z\cdot B_r - r\cdot B_z)$$
(3b)

$$\frac{\partial}{\partial t}(mz) = -e(E_z + r \cdot B_\theta - \theta \cdot B_r) \tag{3c}$$

Where the dots indicate differentiation concerning time. Let $u=v\gamma$ with components u_r , u_{θ} and u_z . Equation (3) can be rewritten in the following form:

$$\frac{dU_r}{dt} + \frac{U_{\theta}^2}{\gamma_{ral}r} = -\frac{e}{m_0} \left(E_r + \frac{U_{\theta}B_z}{\gamma_{ral}} - \frac{U_zB_{\theta}}{\gamma_{ral}} \right)$$
(4a)
$$\frac{dU_{\theta}}{\eta_{ral}} + \frac{U_{\theta}U_r}{\eta_{ral}} = -\frac{e}{m_0} \left(E_{\theta} + \frac{U_zB_r}{\eta_{ral}} - \frac{U_rB_z}{\eta_{ral}} \right)$$
(4b)

$$\frac{dt}{dt} + \frac{\gamma_{ral}r}{\gamma_{ral}} = -\frac{e}{m_0} \left(E_z + \frac{U_r B_\theta}{\gamma_{ral}} - \frac{U_\theta B_r}{\gamma_{ral}} \right)$$
(10)
(4c)

It is convenient to introduce a normalization scheme by which the cavity radius (R_0) is scaled out of Equation (4). This can be achieved through the following procedure[8] Length normalization to $R_0 = \left(r = \frac{r}{R_0}\right)$, Time normalized to $\frac{R_0}{c}\left(\bar{t} = \frac{tc}{R_0}\right)$ Frequency normalized to), $\frac{c}{R_0}\left(\bar{W} = \frac{wR_0}{c}\right)$ Velocity normalized to c $\left(\bar{v}\frac{v}{c}\right)$, Electric field normalized to $\frac{m_0c}{eR_W}\left(\bar{E} = \frac{EeR_0}{m_0c^2}\right)$, Magnetic field normalized to $\frac{m_0c}{eR_W}\left(\bar{E} = \frac{EeR_0}{m_0c^2}\right)$

$$k_c = \frac{x_{mn}}{R_0} = k_\perp$$
(5)

Where xmn is the nth-non van shining root of j(x)=0 Hence, the RF-field components of the TEmn -modes, using the laboratory frame of references, are: Equation (4) may be rewritten in the following form:

$$\frac{d\bar{U}_r}{dt} = \frac{\bar{U}_{\theta}^2}{\gamma_{ral}\bar{r}} - \bar{E}_r - \frac{(\bar{U}_{\theta}\bar{B}_z - \bar{U}_z\bar{B}_{\theta})}{\gamma_{ral}}$$
(6a)

$$\frac{d\overline{\upsilon}_{\theta}}{dt} = \frac{\overline{\upsilon}_{\theta}\overline{\upsilon}_{r}}{\gamma_{ral}\overline{r}} - E_{\vartheta} - \frac{(\overline{\upsilon}_{z}\overline{B}_{r} - \overline{\upsilon}_{r}\overline{B}_{z})}{\gamma_{ral}}$$
(6b)

$$\frac{d\bar{U}_z}{dt} = -\bar{E}_r - \frac{(\bar{U}_r\bar{B}_\vartheta - \bar{U}_\theta\bar{B}_r)}{\gamma_{ral}}$$
(6c)

The normalized perpendicular velocity-time, relativistic is: $U_{\perp} = (U_{\theta} + U_r)^{\frac{1}{2}}$ Let Λ is the angle between $\overline{U_{\perp}}$ and $\overline{U_r}$, hence:

$$U_r = U_{\perp} \cos(^{\wedge}), U_{\theta} = U_{\perp} \sin^{\wedge}$$
⁽⁷⁾
⁽⁴⁾
⁽⁴

$$\frac{d^{\wedge}}{dt} = -\left(E_r \cos(\gamma) + E_{\theta} \sin(\gamma) + B_{\theta} \sin(\gamma) + B_{\theta} \sin(\gamma) \frac{1}{\gamma_{ral}}\right)$$

$$\frac{d^{\wedge}}{dt} = -\frac{U_{\perp} \sin^{\wedge}}{2} + \frac{E_r \sin^{\wedge} - E_{\theta} \cos^{\wedge}}{2} - \frac{U_z (B_{\theta} \sin(\gamma) + B_r \sin^{\wedge})}{2}$$
(8b)

$$\begin{array}{ccc} dt & \gamma_{ral}r & U_{\perp} & \gamma_{ral}U_{\perp} \\ \frac{dU_z}{dt} = -(E_r + U_{\perp}(B_\theta\cos(\wedge)) - B_r\sin(\wedge)) \end{array}$$

$$(8c)$$

Equation (8) represents the electron components. If the radiation wave is a summed to propagate in the positive (z)-direction, the Doppler-shifted electron angular frequency (or Gyro-frequency of the propagating wave is defined as:

$$\Omega_D = k_z v_z + \frac{\Omega_e}{\gamma_{ral}} \tag{9}$$

Where $k_z v_z$ is Doppler term, $v_z is$ the axial drift velocity of the electron, $\Omega_e = \frac{eB_0}{m}$ is non-relativistic gyro- frequency of the electron, where B_0 Represent external magnetic field flux density:

 $\gamma_{ral} = \left[1 - \frac{v_{\perp}^2 + v_{\ell}^2}{c^2}\right]^{\frac{-1}{2}}$ is the relativistic factor, v_{\perp} is azimuthally component of the electron drift velocity, v_{ℓ} is an axial component of the electron drift velocity, the instantaneous value of the Ω_D can be expressed. The total efficiency of the gyrotron interaction can be written as [9].

$$\eta_{\perp} = \left(1 - \frac{Q}{Q_{ohm}}\right) \frac{\beta_{\perp}^2}{2\left(1 - \frac{1}{\gamma}\right)} \eta_{\perp} \tag{10}$$

3. RESULTS AND DISCUSSION

A computer program (Gyro) was constructed to design the cavity and to study the wave-particle interaction inside the cavity. This code uses the forward finite difference technique as a numerical

method for solving all governing differential equations (6 and 8) in three dimensions (r, ϕ, z) for each time step in the beam reference frame (BRF). The input data of the program are electron energy, the velocity ratio, normalized cavity length, normalized value of the external magnetic field, the mode number (m,n,l), and nth-non van shining root of $J'_m(x) = 0$. While the program calculates the initial electron guiding center position using Equation (5). It computes at each time step the electron position in (r, ϕ ,z) and its energy, and the efficiency from equation(10). From the experimental start, current values of seven observed modes and nonlinear modeling have been performed using the timedependent simulation code MAGY compared with values calculated in [11], [13].See Fig.4 show the competition of mode in cavity at 460GHz.



Figure 2: Start oscillation current data versus flux density for second harmonic TE₀₆₁ mode from in the range (8.3T to 8.4T)



Figure 3: Start oscillation current data versus magnetic flux density for second harmonicTE₂₆₁ mode from (8.33T to 8.355T)



Figure 4: indicates the competing second harmonic (TE₀₆₁ and TE₂₆₁) modes with the dominant mode in gyrotron at 460 GHz.



Figure 5: The relation between and magnetic field for the TE_{061} mode



Figure 6: Frequency of the TE_{0,6}-mode as a function of mode with the main magnetic field

Figure (4,5) show study the effect of the tapering magnetic

TE _{mnl} mode	Bo	I _{St}	f	$B_0(T)$	I _{St}	f	$B_0(T)$	f	I _{st}
	(T)	(mA)	(GHz)	Exp.[10,12]	(mA)	(GHz)	Theory	(GHz)	(mA)
							[13,14]		
TE ₂₂₁	5.84	4	157.06	5.747	4	156.9	5.746	156.8	4
	8					0		9	
TE_{421}	8.45	2	217.30	7.933	2	217.1	7.926	217.0	4
						0		9	
TE ₀₆₁	13.4	18	459.14	8.388	67	458.5	8.390	456.1	67
	0					6		5	
TE ₂₃₁	8.35	18	233.44	8.454	18	233.1	8.433	233.1	27
	9					5		5	
TE_{031}	8.62	10	238.24	8.625	16	237.9	8.605	237.9	7
	0		5			1		2	
TE ₅₂₁	8.59	13	246.31	8.936	7	246.0	8.915	246.0	14
	1		5			0		1	

TABLE I: comparisons of the output of the constructed program with those of the reference

 TABLE II: comparisons of the outputs of the constructed program with those of the reference [15]

Item	Research result	Ref [15]
Frequency	459.22	460
Magnetic field	8.3899 T	8.4 T
Harmonic number	2	2
Mode	0, 6, 1	0,6,1
Accelerating voltage	12 Kv	12 kV
Beam current	120 Ma	100 mA
Velocity path factor	2	2
Electron beam radius	1.0 mm	1.0 mm
Cavity diffractive Q	31.100	31.100
Cavity ohmic Q	19.400	19.400
Total cavity	12.000	12.000

4. CONCLUSION

The gyrotron (460 GHz) can efficiently produce at the second harmonic in low voltage.12-kV, 100 mA electron beams and the magnetic field applied was 8.7 to study of the harmonic design mode. The minimum starting current of TE-mode is 18mA, agreeing with the linear theory prediction. The gyrotron is currently being processed for cyclotron wave second-harmonic generation at 460 GHz. The values of the starting current vary by changing the applied external magnetic field, and their values are very important for the excitation of modes.

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References

[1] F.C.de Lucia, "Science and technology in the sub millimeter region," Optics and photonics News, Vol. 14, No.8, 2003.

[2] D. Van der Wide, "Applications and outlook for electronic terahertz technology," Optics and Photonics News, 14(4), pp.44-50, 2003.

[3] R. Callis ,W. Cary, S.Chu, J.Doane, R.Ellis, K.Felch,Y.Gorelov, HGrunloh, J.Hosea, K.Kajiwara, J.Lohr, T.Luce, J.Peavy, R. Pinsker , D. ponce, R. P. Rater, M. Shapiro, R. Temkin , and J. Tooker, "Maturing ECRF technology for plasma control," Nuclear Fusion, 43(11), pp.798-807, 2003.

[4] K. Felch , B. Danly , H. Jory , K. Kreischer , W. Lawson, B. Lawson, B. Lawson, B. Levush , and R. temkin "Characteristics and applications of fast-wave gyro devices," Proceedings of the IEEE, Vol. 87, No. 5, pp.752-781,1999.

[5] T. Idehara, I.Ogawa, S.Mitsudo, M.Pereyslavets, N.Nishida, and K.Yoshida, "Development of frequency tunable, medium power gyrotrons (gyrotron FU series) as sub millimeter wave radiation sources," IEEE Trans. on Plasma Sci., vol. 27, No. 2, pp.340-354, 1999.

[6] H. Li, Z.Xie, W.Wang, Y. Luo, P. Du, X.Den, H.Wang, S.Yu, X.Niu, L.Wang, and S.Liu., "A 35-GHz Low-voltage third-harmonic gyrotron with a permanent magnet system," IEEE Trans. Plasma Sci., vol.31, No.2, pp.264-271, 2003.

[7] V. Bajaj, C.Farrar, M. Hornstein, I. Mastovsky, JVieregg, J.Bryant, B.Elena, K.Kreischer, R.Temkin, and R.Griffin" "Dynamic nuclear polarization at 9 Tesla using a novel 250 GHz gyrotron microwave source", J. Mag. Res, 160(2), pp.85-90, Feb.2002.

[8] Kwo Ray Chu Michael .E. Read and Achintya K. Ganguly . "Method of efficiency enhancement and scaling for the gyrotron oscillator," IEEE Transaction on Microwave theory and Techniques, Vol-MTT-28, No.4, pp.318-324, 1980.

[9] Nguyen, and Victor L. Granatstien, "Nonlinear theory of the Gyro-TWT: comparison of analytical method and numerical code data for the NRL Gyro-TWT," IEEE transaction on plasma sciences, Vol. 30 No. 3, pp. 1186-1195, 2002.

[10] S. Chosh et al. "A new approach for dispersion characteristics and Interaction Impedance for a helical slow- wave structure used in a practical TWT," IEEE Journal of Research, Vol. 47, No. 3&4, pp. 145 -151, 2001.

[11] M. Yeddulla, G. Nusinovich and T. Antonsen, "Start currents in an over mode gyrotron," Phys. Plasmas, Vol.1, No 11, pp.4513-4520, 2003.

[12] Kreischer K, D, B, Woskoboinikow, P, Muligan W, Temkin R "Frequency pulling and band width measurements of a 140GHz Pulsed gyrotron," In J Elec Dec; 57(6) 851-862, 1984.

[13] Hornstein et al. "Continuous- wave operation of a 460-GHz second harmonic gyrotron oscillator," IEEE transaction on plasma sciences, Vol. 34, No. 3, pp.524-533, 2006.

[14] M. K. Hornstein et al., "Second harmonic operation at 460 GHz and broadband continuous frequency tuning of a gyrotron oscillator," EEE transaction on Electron Devices, 2004.

[15] Milissa K. Hornstein, "Design of 460 GHz Second harmonic gyrotron for use in dynamic nuclear polarization," M.Sc. Thesis, Massachusetts Institute of Technology. Cambridge USA, Massachusetts 2001

<u>Appendix1</u>

PROGRAM MODE_TE_061 PARAMETER (IMAX=15, JMAX=15)

```
COMMON/MES/X(0:IMAX+1,0:JAMX+1)
OPEN (UNIT=2,FILE='XM.DAT')
OPEN (UNIT=6,FILE ='OUT-LT2.OUT')
OPEN (UNIT=8,FILE='OUTAM1.OUT')
OPEN (UNIT=9, FILE='OU1.OUT')
X(0,6)=9.8086
WRITE (6,*) X(0,6)
DO 1 I=1, 13
READ (2,*) M,N,L,XN,AL,ALPHA,Q
XMN1=X(M,N)
!.....
CALL α Factor (XMN1, FMN, BD1, DOL1, IST, PW, η)
!.....
END DO
1
END PROGRAM
```