# Improving the Metal Removal Rate (MRR) in Electro Discharge Machining by Additives Powder

Dr. Saad Kariem Shather Production and Metallurgy Engineering Department, University of Technology/Baghdad Ruaa Amer salim Production and Metallurgy Engineering Department, University of Technology/Baghdad Email: roro\_prde@yahoo.com

Received on:19/5/2015 & Accepted on:9/3/2016

### ABSTRACT

Electro discharge machining (EDM) is one of non-traditional machining processes which is used in important application. This paper has focused on improving material removal rate by adding powders (Al<sub>2</sub>O<sub>3</sub> particle size 15-35 $\mu$ m) and (SiO<sub>2</sub> particle size 20-30 $\mu$ m) to kerosene solution through EDM process with different ratios (0.1, 0.14, 0.18 to 0.25 g) particle size for each liter using different values of currents (8, 16 and 30 Amp) and (140 Volt) and (Toff, Ton 25 and 37  $\mu$ Sec),

Medium carbon steel is used as a workpeice and copper as electrode, the material removal rate (MRR). It has been found that maximum MRR was (0.2969) g/min when adding SiO<sub>2</sub> powder (0.25)g/l and maximum MRR was (0.2781)g/min when adding Al<sub>2</sub>O<sub>3</sub> powder (0.25)g/l, the Minitab model program was used to predict the MRR which gives a good result and agreement with experiments 99%.

**Keywords:-**  $Al_2O_3$ ,  $SiO_2$ , EDM, material removal rate (MRR), Estimation of Optimum Response Characteristics for (MRR).

## **INTRODUCTION**

DM is a non-conventional manufacturing process. In this process, the material is removed by erosive action of electric discharges occurring between a tool electrode and workpiece based I on the fact that no tool force is generated during machining. Both workpiece and tool electrode are submerged in a solution called dielectric. The mechanical characteristics of workpiece and electrode are not a concern because the electrical energy is converted into thermal energy causing melting of the material. EDM process allows the machining of hard materials and more complex shapes which cannot be processed by other conventional methods. The EDM process is normally applied to mould and die making. Compared to conventional machining method, the material removal rate of this machining remains rather low [1]. EDM is a process of removing material in a closely controlled manner from an electrically conductive material immersed in a liquid dielectric by a series of randomly distributed discrete electrical sparks or discharges. Nonconducting materials cannot act directly on electrode to achieve EDM. In order to machine these materials with EDM, the conditions that electrical discharges can be produced on their surface must be created [2]. The process also has the advantage of being able to machine hardened tool steels. However, its low machining efficiency and poor surface finish restricted its further applications [3]

Lazerenko and the people who have invented the relax action circuit; they have invented a simple servo controller that helps to maintain the gap width between the tool and workpiece. This reduced arcing and made EDM machining more profitable [4, 5, and 6].

2766

2412-0758/University of Technology-Iraq, Baghdad, Iraq

This is an open access article under the CC BY 4.0 license http://creativecommons.org/licenses/by/4.0

#### **Experimental Work**

The experiments have been conducted using the Electric Discharge Machine, model (CM 323C+50N) (die sinking type), the polarity of the electrode has been set as negative while that of workpiece is positive. The dielectric fluid used is EDM kerosene. Then used glass pool that has dimensions (350,200,220) mm and putting it inside the container EDM machine motor for keeping the kerosene in the case of moving and making a workpiece holder from Teflon to fix the sample, the wire diameter (6mm) was used between a workpice holder and the table of EDM machine to contact the electrical to sample.

**Workpiece**: - medium carbon steel was used as workpieces and the chemical composition is shown in table.

C%	SI%	Mn%	P%	S%	Cr%	Mo%	Ni%	AL%	Co%	Cu%	V%	Fe%
0.415	0.205	0.655	0.006	0.008	0.036	0.02	0.071	0.003	0.006	0.099	0.0005	98.4

Table (1) The chemical compositions of workpiece

•Chemical tests were made by the (S.I.E.R) State Company for Inspection and Engineering Rehabilitation.

•Electrode (Copper) : The copper which is used in experiments has the following chemical composition as shown in table (2)

Table (2) chemical composition of copper

Zn%	Pb%	Sn%	P%	Mn%	Fe%	Na%	Si%	Mg%	Cr%	Al%	S%	C%	Cu%
0.057	0.001	0.005	0.002	0.0005	0.012	0.001	0.001	0.0001	0.0009	0.008	0.005	0.004	99.9

Powder:- Two types of powder used in experiments ( $Al_2O_3$  and  $SiO_2$ ) and the particle size for ( $Al_2O_3$ ) was (15-30µm) and for (SiO<sub>2</sub>) was (20-30 µm).

(MRR):- Material removal rate can be calculation as follow:-

$$MRR = \frac{Wi - Wi}{T}$$

Where wi- weight of workpiece before machining Wf-weight of workpiece after machining.

#### **Results and Discussions**

The Effect of Current on Metal Removal Rate (MRR) by Using Pulse on Time and Pulse off sample the MRR increased, with pulse on time and pulse of time (25  $\mu$ Sec). Time (25  $\mu$ sec). Sample without additives:

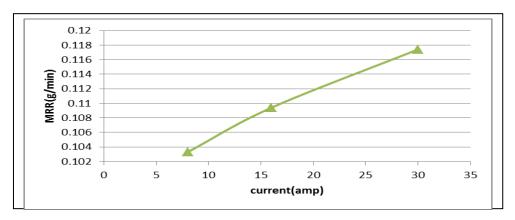


Figure (1) influence of current on MRR

Figure (1) shows the Influence of current on metal removal rate at pulse on (25  $\mu$ Sec) without additives. So When additives powder of(Al<sub>2</sub>O<sub>3</sub>) As shown in Fig (2), with ratio (0.1 g/L) the MRR increase by increasing the current (8, 16 and 30) A, at pulse on time and off time 25  $\mu$ Sec. And by adding (0.14 g/L) Al<sub>2</sub>O<sub>3</sub> noted MRR increase by increasing the current. Also by the same conditions pulse on time and off time 25  $\mu$ Sec, increasing the Al<sub>2</sub>O<sub>3</sub> powder by ratios (0.18 and 0.25) makes it noted that the ratio (0.25) shows greater MRR than the other ratios by adding the current, and this is due to the Al<sub>2</sub>O<sub>3</sub> powder effecting the MRR of the sample comparison with the sample that without additives.

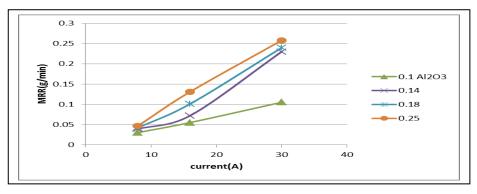


Figure (2) Influence of current on Metal Removal Rate at pulse on and off time 25 (uSec) with additives.Al2O3

and when using powder (SiO<sub>2</sub>) As shown in Fig (3),with ratio (0.1 g/L) the MRR increasing by increase the current (8, 16 and 30) A, at pulse on time and off time 25  $\mu$ Sec. And by adding (0.14 g/L) SiO<sub>2</sub> noted MRR increase by increasing the current. Also by the same conditions pulse on time and off time 25  $\mu$ Sec, increased the SiO<sub>2</sub> powder by ratios (0.18 and 0.25) makes it noted that the ratio (0.25) shows greater MRR than the other ratios by adding the current, and this is due to the SiO<sub>2</sub> powder effecting on the MRR of the sample comparison with the sample that without additives and by comparison of the SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>, it has been noted that the MRR in Al<sub>2</sub>O<sub>3</sub> is less than in SiO<sub>2</sub>, that means the effect of adding Al<sub>2</sub>O<sub>3</sub> in the processing of EDM is better than SiO<sub>2</sub>.

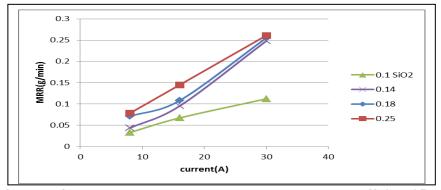


Figure (3) influence of current on metal removal rate at pulse on and off time 25 µSec with additives SiO2

The influence of current on Metal Removal Rate at pulse on and off time of 25 ( $\mu$ Sec) with additives was used for the estimation of Optimum Response Characteristics for Material Removal Rate (MRR) Without Adding Powder.

Figure (4) shows the graph of effects Plot of machining factors, the first response (MRR) for mean, and table (3) shows the results of means. What is shown in this table, are all the selected four parameters of concentration of powder (A), current (B), pulse on (C) and pulse off (D). It is clear that the optimal parametric combination for maximum MRR is  $A_1B_3C_2D_2$ , i.e., at (30Amp) current , (37µsec) Ton and (37 µsec)Toff. . It is suggested that the parametric combination within the considered range as mentioned above gives greater material removal rate (MRR). Using these data, the optimum material removal rate (MRR) can be predicted using the optimum machining conditions mentioned above and according to the relation:

Predicted Mean (MRR) =  $A_1 + B_3 + C_2 + D_2 - 3$ (average mean)

Where:  $A_1$  = Average of (MRR) at the first level of concentration of powder

 $B_3$  = Average of (MRR) at the third level of current

 $C_2$ = Average of (MRR) at the second level of Ton

 $D_2$ = Average of (MRR) at the second level of Toff

From Table (3):Predicted Mean (MRR) = 0.1399+0.2020 + 0.1696 + 0.1696-3 \*(0.13986)



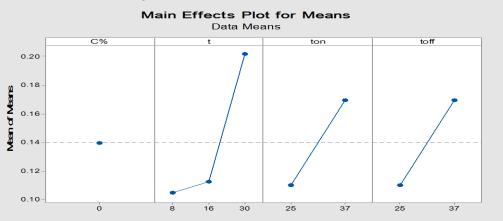


Figure (4) Main effects Plot for means for material removal rate.

NO.	C%	t	Ton	Toff	MRR1	MRR2	MRR3	SNRA	MEAN			
1	0	8	25	25	0.1033	0.1033	0.1033	-19.71	0.1033			
2	0	8	37	37	0.1069	0.1069	0.1069	-19.42	0.1069			
3	0	16	25	25	0.1096	0.1096	0.1096	-19.20	0.1096			
4	0	16	37	37	0.1154	0.1154	0.1154	-18.75	0.1154			
5	0	30	25	25	0.1174	0.1174	0.1174	-18.60	0.1174			
6	0	30	37	37	0.2866	0.2866	0.2866	-10.85	0.2866			

Table (3):L6 TOA

Table (4)	Response	Tabl	e for	Means of	f materia	l removal	l rate
-----------	----------	------	-------	----------	-----------	-----------	--------

Level	C%	t	Ton	Toff
1	0.1399	0.1051	0.1101	0.1101
2		0.1125	0.1696	0.1696
3		0.2020		
Delta	0.0000	0.0969	0.0595	0.0595
Rank	4	1	2.5	2.5

Estimation of Optimum Response Characteristics for Material Removal Rate (MRR) with Adding  $Al_2O_3$ 

Figure (4) shows the graph of effects Plot of machining factors, the first response (MRR) for mean and table (6) shows the results of means. What is shown in this table are all the selected four parameters of concentration of  $Al_2O_3$  powder (A), current (B), pulse on (C) and pulse off (D). It is clear that the optimal parametric combination for maximum MRR is  $A_4 B_3 C_2D_2$ , i.e., at 0.25 g/l  $Al_2O_3$  powder, (30Amp) current, (37µsec) Ton and (37µsec)Toff. . It is suggested that the parametric combination within the considered range as mentioned above gives greater material removal rate (MRR). Using these data, the optimum material removal rate (MRR) can be predicted using the optimum machining conditions mentioned above and according to the relation:

Predicted Mean (MRR) =  $A_4 + B_3 + C_2 + D_2 - 3$ (average mean)

Where

A<sub>4</sub>= Average of (MRR) at the fourth level of concentration of Al<sub>2</sub>O<sub>3</sub> powder

 $B_3$ = Average of (MRR) at the third level of current

 $C_2$ = Average of (MRR) at the second level of Ton

 $D_2$  = Average of (MRR) at the second level of Toff

From Table (4):

Predicted Mean (MRR)=0.16488+0.22643 + 0.14757 +0.14757-3 \*(0.129644) = 0.29751675 g/min

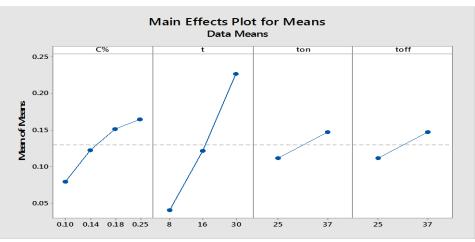


Figure (5) Main effects Plot for means for material removal rate

	<b>Table (5): L<sub>24</sub> TOA</b>											
NO.	C%	t	Ton	Toff	MRR1	MRR2 2	MRR3	SNRA1	MEAN1			
1	0.1	8	25	25	0.0305	0.0305	0.0305	-30.31	0.0305			
2	0.14	8	25	25	0.039	0.039	0.039	-28.17	0.039			
3	0.18	8	25	25	0.042	0.042	0.042	-27.53	0.042			
4	0.25	8	25	25	0.0466	0.0466	0.0466	-26.63	0.0466			
5	0.1	16	25	25	0.05	0.05	0.05	-26.02	0.0501			
6	0.14	16	25	25	0.072	0.072	0.072	-22.85	0.072			
7	0.18	16	25	25	0.1011	0.1011	0.1011	-19.90	0.1011			
8	0.25	16	25	25	0.131	0.131	0.131	-17.65	0.131			
9	0.1	30	25	25	0.105	0.105	0.105	-19.57	0.105			
10	0.14	30	25	25	0.23	0.23	0.23	-12.76	0.230			
11	0.18	30	25	25	0.238	0.238	0.238	-12.46	0.238			
12	0.25	30	25	25	0.255	0.255	0.255	-11.86	0.255			
13	0.1	8	37	37	0.0349	0.0349	0.0349	-29.14	0.0349			
14	0.14	8	37	37	0.04	0.04	0.04	-27.95	0.0400			
15	0.18	8	37	37	0.045	0.045	0.045	-26.93	0.04505			
16	0.25	8	37	37	0.0486	0.0486	0.0486	-26.26	0.0486			
17	0.1	16	37	37	0.0777	0.0777	0.0777	-22.19	0.0777			
18	0.14	16	37	37	0.098	0.098	0.098	-20.17	0.09802			
19	0.18	16	37	37	0.2133	0.2133	0.2133	-13.42	0.213296			
20	0.25	16	37	37	0.23	0.23	0.23	-12.76	0.2300			
21	0.1	30	37	37	0.18	0.18	0.18	-14.89	0.1802			
22	0.14	30	37	37	0.2562	0.2562	0.2562	-11.82	0.2562			
23	0.18	30	37	37	0.2691	0.2691	0.2691	-11.40	0.269			
24	0.25	30	37	37	0.2781	0.2781	0.2781	-11.11	0.2781			

fable (	(5):	La	TOA
	J		

level	C%	t	Ton	Toff								
1	0.07968	0.04083	0.11168	0.11168								
2	0.12253	0.12164	0.14757	0.14757								
3	0.15142	0.22643										
4	0.16488											
Delta	0.08520	0.18560	0.03589	0.03589								
rank	2	1	3.5	3.5								

Table (6): Res	sponse Table f	for Means of	' materia	l removal rate
----------------	----------------	--------------	-----------	----------------

Estimation of Optimum Response Characteristics for Material Removal Rate (MRR) with Adding  $SiO_2$ 

Figure (5) shows the graph of effects Plot of machining factors, the first response (MRR) for mean and table (8) shows the results of means. What is shown in this table are all the selected four parameters of concentration of SiO<sub>2</sub> powder (A), current (B) , pulse on (C) and pulse off (D). It is clear that the optimal parametric combination for maximum MRR is  $A_4B_3C_2D_2$ , i.e., at 0.25 g/l  $Al_2O_3$  powder, (30Amp) current , (37µsec) Ton and (37 µsec)Toff. . It is suggested that the parametric combination within the considered range as mentioned above gives greater material removal rate (MRR). Using these data , the optimum material removal rate (MRR) can be predicted using the optimum machining conditions mentioned above and according to the relation: Predicted Mean (MRR) =  $A_4 + B_3 + C_2 + D_2 - 3$ (average mean)

Where

 $A_4$ = Average of (MRR) at the fourth level of concentration of SiO<sub>2</sub> powder

 $B_3$  = Average of (MRR) at the third level of current

 $C_2$ = Average of (MRR) at the second level of Ton

 $D_2$ = Average of (MRR) at the second level of Toff

From Table (6):

Predicted Mean(MRR) = 0.18298+0.23959+ 0.16263+0.16263-3 \*(0.1433)

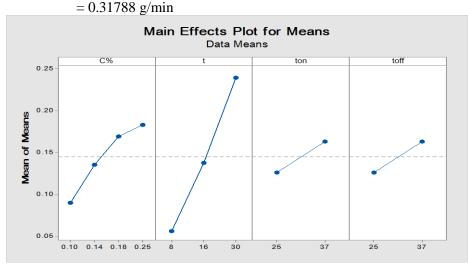


Figure (7) Main effects Plot for means for material removal rate

Table (7):L <sub>24</sub> TOA											
NO.	C%	t	Ton	Toff	MRR1	MRR2	MRR3	SNRA	MEAN		
1	0.10	8	25	25	0.0329	0.0329	0.0329	-29.65	0.0329		
2	0.14	8	25	25	0.0434	0.0434	0.0434	-27.25	0.0434		
3	0.18	8	25	25	0.0710	0.0710	0.0710	-22.97	0.0710		
4	0.25	8	25	25	0.0722	0.0722	0.0722	-22.82	0.0722		
5	0.10	16	25	25	0.0670	0.0670	0.0670	-23.47	0.0670		
6	0.14	16	25	25	0.0950	0.0950	0.0950	-20.44	0.0950		
7	0.18	16	25	25	0.1078	0.1078	0.1078	-19.34	0.1078		
8	0.25	16	25	25	0.1457	0.1457	0.1457	-16.73	0.1457		
9	0.10	30	25	25	0.1121	0.1121	0.1121	-19.00	0.1121		
10	0.14	30	25	25	0.2491	0.2491	0.2491	-12.07	0.2491		
11	0.18	30	25	25	0.2561	0.2561	0.2561	-11.83	0.2561		
12	0.25	30	25	25	0.2630	0.2630	0.2630	-11.60	0.2630		
13	0.10	8	37	37	0.0358	0.0358	0.0358	-28.92	0.0358		
14	0.14	8	37	37	0.0440	0.0440	0.0440	-27.13	0.0440		
15	0.18	8	37	37	0.0741	0.0741	0.0741	-22.60	0.0741		
16	0.25	8	37	37	0.0760	0.0760	0.0760	-22.38	0.0760		
17	0.10	16	37	37	0.0900	0.0900	0.0900	-20.91	0.0900		
18	0.14	16	37	37	0.1211	0.1211	0.1211	-18.33	0.1211		
19	0.18	16	37	37	0.2301	0.2301	0.2301	-12.76	0.2301		
20	0.25	16	37	37	0.2441	0.2441	0.2441	-12.24	0.2441		
21	0.10	30	37	37	0.2023	0.2023	0.2023	-13.88	0.2023		
22	0.14	30	37	37	0.2602	0.2602	0.2602	-11.69	0.2602		
23	0.18	30	37	37	0.2770	0.2770	0.2770	-11.15	0.2770		
24	0.25	30	37	37	0.2969	0.2969	0.2969	-10.54	0.2969		

## Table (8): Response Table for Means of material removal rate

Level	C%	t	Ton	Toff
1	0.09002	0.05617	0.12628	0.12628
2	0.13547	0.13760	0.16263	0.16263
3	0.16935	0.23959		
4	0.18298			
Delta	0.09297	0.18341	0.03636	0.03636
Rank	2	1	3.5	3.5

### CONCLUSIONS

The mains conclusions which can be deduced from the present work can be summarized as follows:

- 1. Increasing the current (8, 16 and 30) Amp will increase the MRR.
- 2. Increasing the pulse on and off time increases the MRR.
- 3. The better ratio of  $Al_2O_3$  to maximum MRR is (0.25g), where the (MRR=0.2781 g/min).
- 4. The better ratio of  $SiO_2$  to maximum MRR is (0.25g), where the (MRR=0.2969 g/min).

#### REFERENCES

[1] W.S. Zhao, Q.G. Meng, Z.L. Wang, The application of research on powder mixed EDM in rough machining, J. Mater. Process. Technol.

129 (2002) 30–33.

[2] Davis, Joseph R. ASM HANDBOOK, Volume 16 Machining- Published: 1989.

[3]Jayakumar, N., et al, Tool wear compensation and path generation in micro and macro EDM,

Journal of Manufacturing Processes, University of Nebraska-Lincoln, Vol. 32, 2004.

[4]R.Rajesha and M. Dev Anandb ,"The Optimization of the Electro-Discharge Machining Process Using Response Surface Methodology and Genetic Algorithms", Department of Mechanical Engineering, India , International Conference on Modelling, Optimization and Computing, 2012.

[5] Lotfi, K., G., "Electrical Discharge Machining (EDM)", the American

University in Cairo, Department of Mechanical Engineering, Vol. 202, 2003.

[6]Shanker Singh, S. Maheshwari& P.C. Pandey."Some Investigations into the Electric Discharge Machining of Hardened Tool Steel Using Different Electrode Materials". Journal of Materials Processing Technology, Vol (149). pp. 272-277,2004.